

**GENERAL APTITUDE****Q. No. 1 - 5 Carry One Mark Each**

1. The minister avoided any mention of the issue of women's reservation in the private sector. He was accused of \_\_\_\_\_ the issue.
- (A) belting                      (B) skirting                      (C) tying                      (D) collaring

**Key: (B)**

2. \_\_\_\_\_ I permitted him to leave, I wouldn't have had any problem with him being absent \_\_\_\_\_ I?
- (A) Had, would                      (B) Have, wouldn't  
(C) Have, would                      (D) Had, wouldn't

**Key: (A)**

3. A worker noticed that the hour hand on the factory clock had moved by 225 degrees during her stay at the factory. For how long did she stay in the factory?
- (A) 3.75 hours                      (B) 7.5 hours  
(C) 4 hours and 15mins                      (D) 8.5 hours

**Key: (B)**

**Sol:** Number of hours in a clock = 12 hours

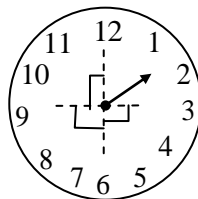
One rotation hour hand covers 360°

360 degree = 12 hours

1 degree =  $\frac{12}{360}$  hours

225° = ?

$$= \frac{12}{360} \times 225 = 7.5 \text{ hours}$$



4. John Thomas, an \_\_\_\_\_ writer, passed away in 2018.
- (A) imminent                      (B) prominent                      (C) dominant                      (D) eminent

**Key: (D)**

5. The sum and product of two integers are 26 and 165 respectively. The difference between these two integers is \_\_\_\_\_.
- (A) 3                                      (B) 6                                      (C) 2                                      (D) 4

**Key: (D)**

**Sol:** Let us take two number are a & b

Given that

$$a + b = 26, ab = 165$$

$$a - b = ?$$

$$(a + b)^2 = 26^2 \Rightarrow a^2 + b^2 + 2ab = 26^2$$

$$a^2 + b^2 = 26^2 - 2ab$$

$$(a - b)^2 = (a^2 + b^2) - 2ab$$

$$(a - b)^2 = 26^2 - 2ab - 2ab$$

$$(a - b)^2 = 26^2 - 4ab \Rightarrow (a - b)^2 = 26^2 - 4 \times 165$$

$$(a - b)^2 = 16 \Rightarrow a - b = 4$$

**Q. No. 6 - 10 Carry Two Marks Each**

6. A person divided an amount of Rs. 100,000 into two parts and invested in two different schemes. In one he got 10% profit and in the other he got 12%. If the profit percentages are interchanged with these investments he would have got Rs. 120 less. Find the ratio between his investments in the two schemes.
- (A) 37:63                                      (B) 9:16                                      (C) 11:14                                      (D) 47:53

**Key: (D)**

**Sol:** Considering first scheme as x second scheme as y

Given that

$$x + y = 1,00,000 \quad \rightarrow (1)$$

Assume profit of sum before interchanging percentage = z

$$1.1x + 1.12y = z \quad \rightarrow (2)$$

After interchanging profit percentages

$$1.12x + 1.1y = z - 120 \quad \rightarrow (3)$$

Solving (2) and (3)

$$1.12x + 1.1y = z - 120$$

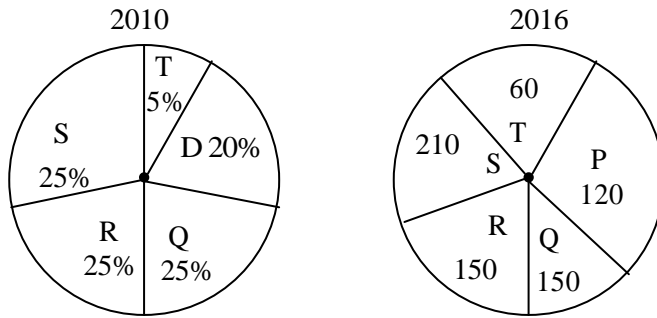
$$1.1x + 1.12y = z$$

$$\begin{array}{r} - \quad - \quad - \\ \hline 0.02x - 0.02y = -120 \end{array}$$



**Key: (D)**

**Sol:**



**In 2010:**

Total number of employees = 600

Number of employees of skills

$Q = R = S = 25\%$  of 600 = 150

Number of employees of skill P = 20% of 600 = 120

Number of employees of skill T = 5% of 600 = 30

**In 2016:**

Total number of employees increased by 15%

Total number of employees =  $1.15 \times 600 = 690$

As there is no change in skill level of P, Q, and R

Number of employees of skill level P = 120

Number of employees of skill level Q = 150

Number of employees of skill level R = 150

Number of employees at skill level S = 40% increases =  $1.4 \times 150 = 210$

Number of employees at skill level T =  $690 - (120 + 150 + 150 + 210) = 60$ .

9. M and N had four children P, Q, R and S. Of them, only P and R were married. They had children X and Y respectively. If Y is a legitimate child of W, which one of the following statement is necessarily FALSE?

(A) M is the grandmother of Y

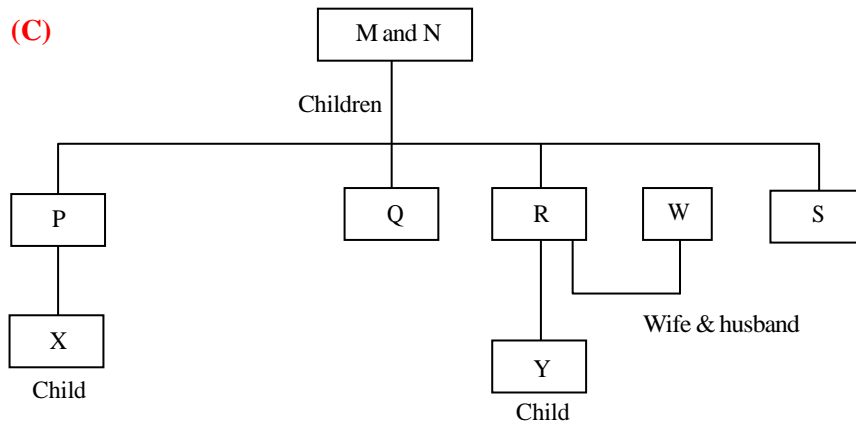
(B) W is the wife of R

(C) W is the wife of P

(D) R is the father of Y

**Key: (C)**

**Sol:**



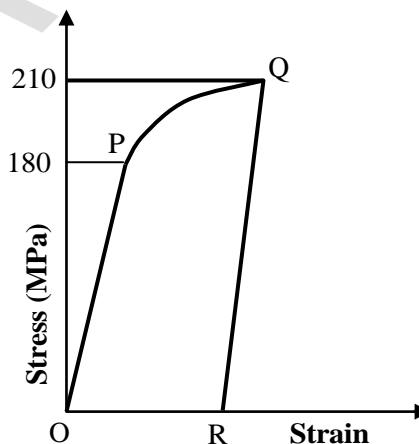
10. Congo was named by Europeans. Congo's dictator Mobutu later changed the name of the country and the river to Zaire with the objective of Africanising names of persons and spaces. However, the name Zaire was a Portuguese alteration of Nzadi o Nzere, a local African term meaning 'River that swallows Rivers'. Zaire was the Portuguese name for the Congo river in the 16th and 17 centuries. Which one of the following statements can be inferred from the paragraph above?
- (A) The term Nzadi o Nzere was of Portuguese origin
  - (B) As a dictator Mobutu ordered the Portuguese to alter the name of the river to Zaire
  - (C) Mobutu's desire to Africanise names was prevented by the Portuguese
  - (D) Mobutu was not entirely successful in Africanising the name of his country

**Key: (D)**

### MECHANICAL ENGINEERING

#### Q. No. 1 to 25 Carry One Mark Each

1. Consider the stress-strain curve for an ideal elastic-plastic strain hardening metal as shown in the figure. The metal was loaded in uniaxial tension starting from O. Upon loading, the stress-strain curve passes through initial yield point at P, and then strain hardens to point Q, where the loading was stopped. From point Q, the specimen was unloaded to point R, where the stress is zero. If the same specimen is reloaded in tension from point R, the value of stress at which the material yields again is \_\_\_\_\_ MPa.



**Key: (210)**

**Sol:** Strain hardening improve tensile strength, yield straight and hardness at the expense of reduced ductility.

2. The length, width and thickness of a steel sample are 400 mm, 410 mm, 40 mm and 20 mm, respectively. Its thickness needs to be uniformly reduced by 2 mm in a single pass by using horizontal slab milling. The milling cutter (diameter: 100 mm, width: 50 mm) has 20 teeth and rotates at 1200 rpm. The feed per tooth is 0.05 mm. The feed direction is along the length of the sample. If the over-travel distance is the same as the approach distance, the approach distance and time taken to complete the required machining task are
- (A) 14mm, 21.4 s      (B) 21 mm, 39.4 s      (C) 21 mm, 28.9s      (D) 14mm, 18.4 s

**Key: (A)**

**Sol:**  $L = 400\text{mm}$

$b = 40\text{ mm}$

$t = 20\text{ mm}$

$d = 2\text{ mm}$

$D = 100\text{ mm}, Z = 20, N = 1200\text{ rpm}$

$f = 0.05\text{ mm/tooth}$

$$C_a = \sqrt{d(D-d)} = \sqrt{2(100-2)} = \sqrt{2 \times 98} = 14\text{ mm}$$

$F = fNZ$

$$= 0.05 \times 1200 \times 20 = 1200\text{ mm/min} = 20\text{ mm/s}$$

$$t_m = \frac{L_e + C_a + C_o}{F} = \frac{400 + 14 + 14}{20} = 21.4\text{ s}$$

3. As per common design practice, the three types of hydraulic turbines, in descending order of flow rate, are
- (A) Francis, Kaplan, Pleton      (B) Kaplan, Francis, Pelton  
(C) Pelton, Kaplan, Francis      (D) Pelton, Francis, Kaplan

**Key: (B)**

**Sol:** Kaplan turbine is operating under high flow rates.

Francis turbine is operating under medium flow rates.

Pelton turbine is operating under low flow rates

4. The table presents the demand of a product. By simple three-months moving average method, the demand-forecast of the product for the month of September is

Month	Demand
January	450
February	440
March	460
April	510
May	520

June	495
July	475
August	560

- (A) 490                      (B) 536.67                      (C) 510                      (D) 530

**Key: (C)**

**Sol:** Forecast of the product of the month September =  $\frac{495 + 475 + 560}{3} = 510$

5. The lengths of a large stock of titanium rods follow a normal distribution with a mean ( $\mu$ ) of 440 mm and a standard deviation ( $\sigma$ ) of 1 mm. What is the percentage of rods whose lengths lie between 438 mm and 441 mm?

- (A) 86.64%                      (B) 68.4%                      (C) 99.75%                      (D) 81.85%

**Key: (D)**

**Sol:** Given, Mean ( $\mu$ ) = 440mm, S.D ( $\sigma$ ) = 1 mm

The random variable 'X' denotes lengths of rods.

$$P[438 < X < 441] = ?$$

The standard normal variable  $Z = \frac{X - \mu}{\sigma}$

$$\text{If } X = 438 \Rightarrow Z = \frac{438 - 440}{1} = -2$$

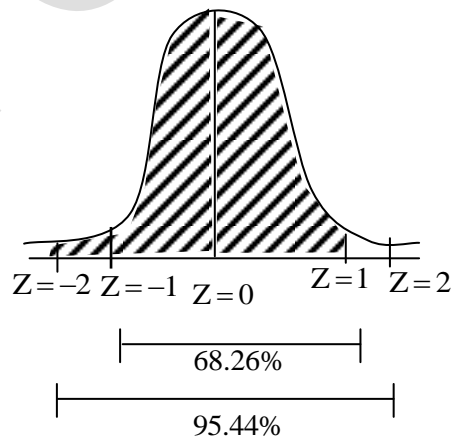
$$\text{If } X = 441 \Rightarrow Z = \frac{441 - 440}{1} = 1$$

$$\therefore P[438 < X < 441] = P[-2 < Z < 1]$$

$$= P[-2 < Z < 0] + P[0 < Z < 1]$$

$$= \left[ \frac{95.44}{2} \right] \% + \left[ \frac{68.26}{2} \right] \% = (47.72)\% + (34.13)\%$$

$$\Rightarrow P[438 < X < 441] = 81.85\%$$



6. During a non-flow thermodynamic process (1-2) executed by a perfect gas, the heat interaction is equal to the work interaction ( $Q_{1-2} = W_{1-2}$ ) when the process is

- (A) Isentropic                      (B) Isothermal                      (C) Polytropic                      (D) Adiabatic

**Key: (B)**

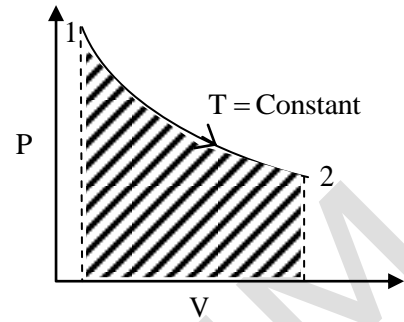
**Sol:** First law of thermodynamics for non flow (closed) system,

$$dQ = du + dW$$

$$\int dQ = \int mc_v dT + \int dW \quad \text{---(1)}$$

When process is isothermal,  $dT = 0 \therefore Q_{12} = W_{12}$

Shaded area shows equal amount of heat & work.



7. Evaluation of  $\int_2^4 x^3 dx$  using a 2-equal-segment trapezoidal rule gives a value of \_\_\_\_\_.

**Key: (63)**

**Sol:** Using Trapezoidal rule, we have

$$\int_a^b f(x) dx \approx \frac{h}{2} [(y_0 + y_n) + 2(y_1 + y_2 + \dots + y_{n-1})];$$

where  $h = \text{step size} = \frac{b-a}{n}$

Let  $f(x) = x^3$ ;  $a = 2$ ;  $b = 4$ ;  $n = \text{number of intervals} = 2$

$$h = \frac{4-2}{2} = 1$$

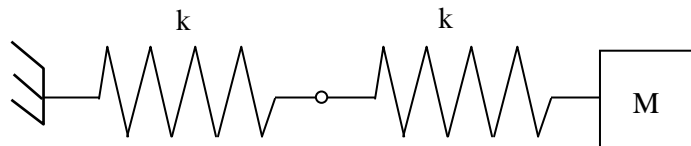
x	2	3	4
$f(x) = x^3$	8	27	64
	$(y_0)$	$(y_1)$	$(y_2)$

$$\therefore \int_2^4 x^3 dx = \frac{1}{2} [(8 + 64) + 2(27)] = \frac{1}{2} [72 + 54] = 63$$

$$\Rightarrow \int_2^4 x^3 dx = 63$$

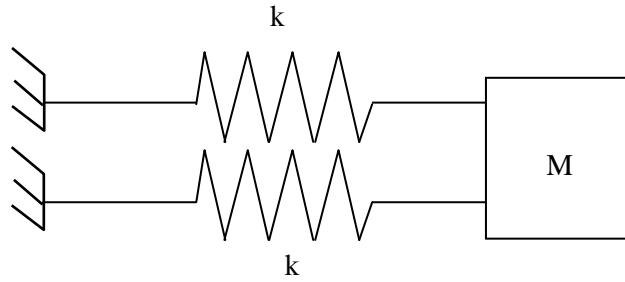
8. The natural frequencies corresponding to the spring-mass systems I and II are  $\omega_I$  and  $\omega_{II}$ ,

respectively. The ratio  $\frac{\omega_I}{\omega_{II}}$  is



**SYSTEM-I**



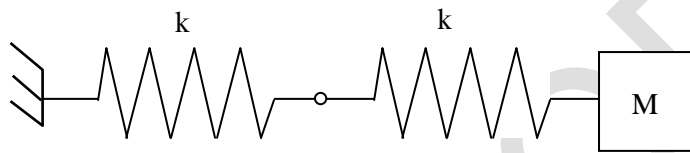


**SYSTEM – II**

- (A)  $\frac{1}{2}$                       (B) 4                      (C) 2                      (D)  $\frac{1}{4}$

**Key: (A)**

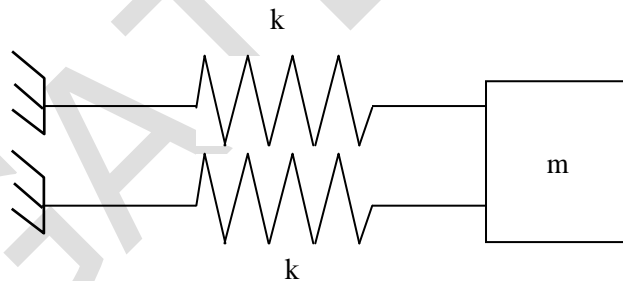
**Sol:**



Since springs are in series

$$\frac{1}{k_{eq}} = \frac{1}{k} + \frac{1}{k} \Rightarrow \frac{1}{k_{eq}} = \frac{2}{k}$$

$$k_{eq} = \frac{k}{2} \text{ and } \omega_1 = \sqrt{\frac{k_{eq}}{m}} = \sqrt{\frac{k}{2m}}$$



Since springs are in parallel  $k_{eq} = k + k \Rightarrow k_{eq} = 2k$

$$\omega_{II} = \sqrt{\frac{k_{eq}}{m}} = \sqrt{\frac{2k}{m}}$$

$$\frac{\omega_I}{\omega_{II}} = \frac{\sqrt{\frac{k}{2m}}}{\sqrt{\frac{2k}{m}}} = \sqrt{\frac{k}{2m}} \times \sqrt{\frac{m}{2k}} = \frac{1}{2}$$

9. A solid cube of side 1 m is kept at a room temperature of  $32^\circ \text{C}$ . The coefficient of linear thermal expansion of the cube material is  $1 \times 10^{-5}/^\circ\text{C}$  and the bulk modulus is 200 GPa. If the

cube is constrained all around and heated uniformly to  $42^\circ\text{C}$ , then the magnitude of volumetric (mean) stress (in MPa) induced due to heating is \_\_\_\_\_.

**Key: (60)**

**Sol:**  $a = 1\text{m}$        $K = 200\text{GPa}$   
 $\Delta T_1 = 32^\circ\text{C}$        $T_f = 42^\circ\text{C}$   
 $\alpha = 1 \times 10^{-5}$        $\sigma_v = ?$   
 $\epsilon_x = \alpha \Delta T = 1 \times 10^{-5} (42 - 32) = 1 \times 10^{-4}$   
 $\epsilon_v = 3 \epsilon_x = 3 \times 10^{-4}$   
 $K = \frac{\sigma_v}{\epsilon_v} \Rightarrow \sigma_v = 3 \times 10^{-4} \times 200 \times 10^3 = 60\text{MPa}$

10. For a hydro dynamically and thermally fully developed laminar flow through a circular pipe of constant cross-section, the Nusselt number at constant wall heat flux ( $Nu_q$ ) and that at constant wall temperature ( $Nu_T$ ) are related as

- (A)  $Nu_q < Nu_T$       (B)  $Nu_q = (Nu_T)^2$       (C)  $Nu_q = Nu_T$       (D)  $Nu_q > Nu_T$

**Key: (D)**

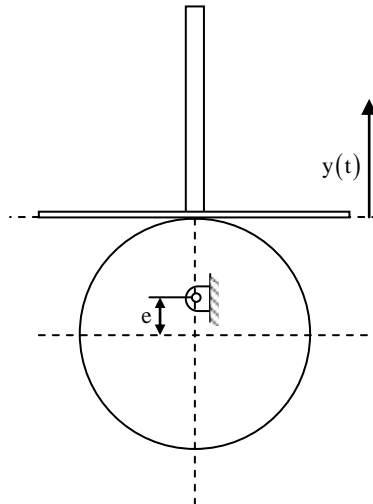
**Sol:** Since average convective heat transfer coefficient ( $\bar{h}$ ) in case of constant heat flux ( $\bar{h}_q$ ) is more than that from constant wall temperature ( $\bar{h}_T$ ).

$$\therefore Nu_q > Nu_T$$

For fully developed laminar flow,

$$Nu_q = 4.36, Nu_T = 3.66$$

11. A flat-faced follower is driven using a circular eccentric cam rotating at a constant angular velocity  $\omega$ . At time  $t = 0$ , the vertical position of the follower is  $y(0) = 0$ , and the system is in the configuration shown below

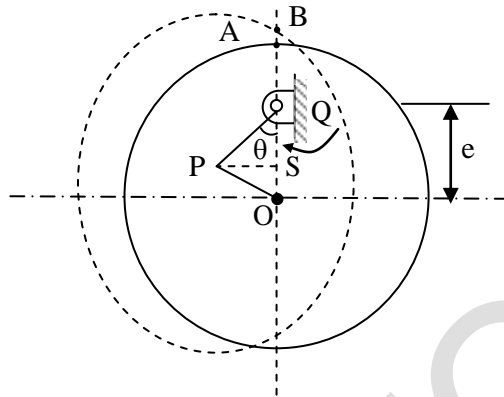


The vertical position of the follower face,  $y(t)$  is given by

- (A)  $e(1 + \cos 2\omega t)$  (B)  $e \sin \omega t$   
 (C)  $e \sin 2\omega t$  (D)  $e(1 - \cos \omega t)$

**Key: (D)**

**Sol:**  $t = 0, y(0) = 0, \omega$



$$\begin{aligned} x &= AB = OS = OQ - QS \\ &= OQ - PQ \cos \theta \\ &= OQ - OQ \cos \theta \\ y &= OQ(1 - \cos \theta) = e(1 - \cos \theta) = e(1 - \cos(\omega t)) \end{aligned}$$

12. In a casting process, a vertical channel through which molten metal and flows downward from pouring basin to runner for reaching the mold cavity is called

- (A) sprue (B) pin hole (C) riser (D) blister

**Key: (A)**

13. Air of mass 1 kg, initially at 300K and 10 bar, is allowed to expand isothermally till it reaches a pressure of 1 bar. Assuming air as an ideal gas with gas constant of 0.287 kJ/kg.K, the change in entropy of air (in kJ/kg.K, round off to two decimal places) is \_\_\_\_\_.

**Key: (0.66)**

**Sol:** Given that for Air, initially  $m = 1\text{kg}, T_1 = 300\text{K}, P_1 = 10 \text{ bar}$

Finally;  $T_2 = 300\text{K}$  (Isothermal)

$$P_2 = 1 \text{ bar}$$

$$R = 0.287 \text{ KJ/kg. K}$$

$$\text{Change in entropy, } \Delta S = m \left[ C_p \ln \frac{T_2}{T_1} - R \ln \frac{P_2}{P_1} \right] \quad \text{---(1)}$$

Since  $T_2 = T_1$

$$\Delta S = -mR \ln \frac{P_2}{P_1} = -1 \times 0.287 \times \ln \frac{1}{10}$$

$$\Delta S = 0.66084$$

$$\Delta S = 0.66 \text{ kJ/kg - K}$$

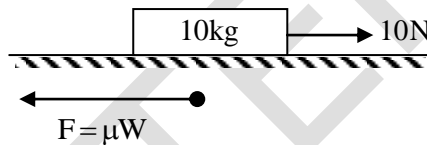
14. A block of mass 10 kg rests on a horizontal floor. The acceleration due to gravity is  $9.81 \text{ m/s}^2$ . The coefficient of static friction between the floor and the block is 0.2.



A horizontal force of 10 N is applied on the block as shown in the figure. The magnitude of force of friction (in N) on the block is \_\_\_\_\_.

**Key: (10)**

**Sol:**  $m = 10\text{kg}$ ,  $\mu = 0.2$ ,  $F = 10\text{N}$   
 $g = 9.81 \text{ m/sec}^2$ ,



$$F = 0.2 \times 10 \times 9.81 \approx 19.62 > 10$$

Hence friction force = 10N.

15. Consider the matrix  $P = \begin{bmatrix} 1 & 1 & 0 \\ 0 & 1 & 1 \\ 0 & 0 & 1 \end{bmatrix}$

The number of distinct eigenvalues of P is

- (A) 0                                      (B) 1                                      (C) 3                                      (D) 2

**Key: (B)**

Given

$$P = \begin{bmatrix} 1 & 1 & 0 \\ 0 & 1 & 1 \\ 0 & 0 & 1 \end{bmatrix}$$

→ Upper triangular matrix

- ∴ Eigen values of P are 1, 1, 1; since the Eigen values of upper triangular matrix are it's diagonal elements.
- ∴ Number of distinct eigen values of P = 1.

16. During a high cycle fatigue test, a metallic specimen is subjected to cyclic loading with a mean stress of +140 MPa, and a minimum stress of -70 MPa. The R-ratio (minimum stress to maximum stress) for this cycle loading is \_\_\_\_ (round off to one decimal place).

**Key: (-0.2)**

**Sol:**  $\sigma_{\text{mean}} = 140\text{MPa}$

$$\sigma_{\text{min}} = -70\text{MPa}; \quad \frac{\sigma_{\text{min}}}{\sigma_{\text{max}}} = ?$$

$$\sigma_{\text{mean}} = \frac{\sigma_{\text{max}} + \sigma_{\text{min}}}{2} = 140$$

$$\sigma_{\text{max}} = 280 + 70 \Rightarrow \sigma_{\text{max}} = 350$$

$$\frac{\sigma_{\text{min}}}{\sigma_{\text{max}}} = \frac{-70}{350} = \frac{-1}{5} = -0.2$$

17. A slender rod of length L, diameter d (L >> d) and thermal conductivity  $k_1$  is joined with another rod of identical dimensions, but of thermal conductivity  $k_2$ , to form a composite cylindrical rod of length 2L. The heat transfer in radial direction and contact resistance are negligible. The effective thermal conductivity of the composite rod is

- (A)  $k_1 + k_2$       (B)  $\sqrt{k_1 k_2}$       (C)  $\frac{2k_1 k_2}{k_1 + k_2}$       (D)  $\frac{k_1 k_2}{k_1 + k_2}$

**Key: (C)**

**Sol:** Two rods of equal length L are conductivity  $k_1$  and  $k_2$  are connected.

No radial heat transfer

∴ Equivalent resistance per unit area

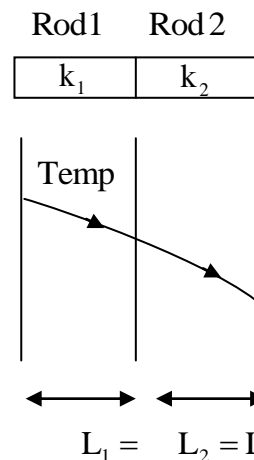
$$R_{\text{eq}} = \frac{L}{k_1} + \frac{L}{k_2} \quad \text{---(i)}$$

If this is single composite rod;

Resistance, of composite rod per unit area

$$R_{\text{comp}} = \frac{2L}{k_{\text{eq}}} \quad \text{---(ii)}$$

From (I) and (II)



$$\frac{2L}{k_{eq}} = \frac{L}{k_1} + \frac{L}{k_2}$$

$$k_{eq} = \frac{2k_1 k_2}{k_1 + k_2}$$

18. Consider an ideal vapor compression refrigeration cycle. If the throttling process is replaced by an isentropic expansion process, keeping all the other processes unchanged, which one of the following statements is true for the modified cycle?

- (A) Coefficient of performance is the same as that of the original cycle
- (B) Coefficient of performance is lower than that of the original cycle
- (C) Refrigerating effect is lower than that of the original cycle
- (D) Coefficient of performance is higher than that of the original cycle

**Key: (D)**

**Sol:** Figure 1: Isenthalpic expansion

Figure 2: Isentropic expansion

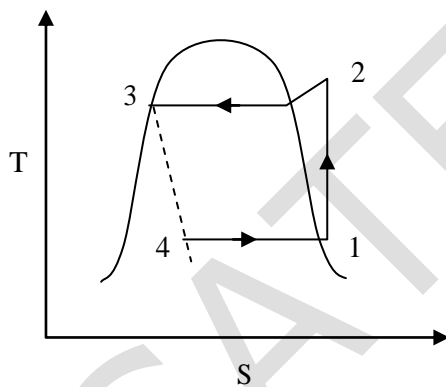


Figure 1

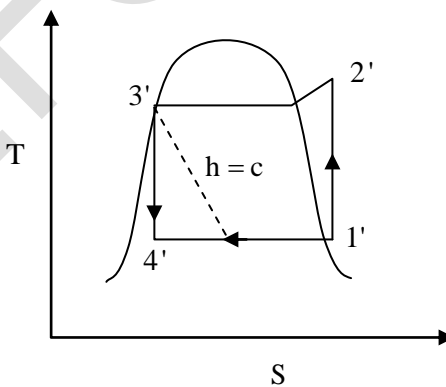


Figure 2

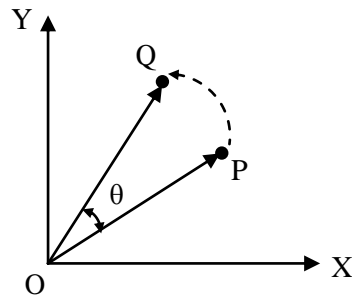
Form both figures we see

$$h_1' - h_4' > h_1 - h_4 \text{ (Refrigerating effect)}$$

∴ COP in case (ii) is more than (i) because of more refrigerating effect.

∴ COP of isentropic expansion is more than isenthalpic expansion.

19. The position vector  $\overline{OP}$  of point P(20, 10) is rotated anti-clockwise in X-Y plane by an angle  $\theta = 30^\circ$  such that point P occupies position Q, as shown in the figure. The coordinates (x, y) of Q are



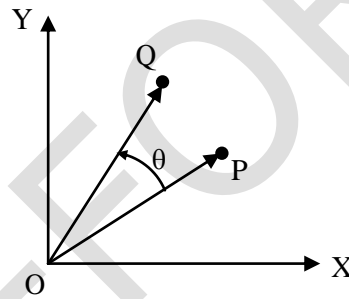
- (A) (13.40, 22.32)      (B) (12.32, 18.66)      (C) (22.32, 8.26)      (D) (18.66, 12.32)

**Key: (B)**

**Sol:**  $P = (20, 10)$ ,  $\theta = 30^\circ$

$Q = (x', y')$

$$\begin{aligned} \begin{bmatrix} x' \\ y' \end{bmatrix} &= \begin{bmatrix} \cos \theta & -\sin \theta \\ \sin \theta & \cos \theta \end{bmatrix} \begin{bmatrix} 20 \\ 10 \end{bmatrix} \\ &= \begin{bmatrix} \sqrt{3}/2 & -1/2 \\ 1/2 & \sqrt{3}/2 \end{bmatrix} \begin{bmatrix} 20 \\ 10 \end{bmatrix} \\ &= \begin{bmatrix} 0.866 & -0.5 \\ 0.5 & 0.866 \end{bmatrix} \begin{bmatrix} 20 \\ 10 \end{bmatrix} = \begin{bmatrix} 12.32 \\ 18.66 \end{bmatrix} \\ (x', y') &= (12.32, 18.66) \end{aligned}$$



20. A cylindrical rod of diameter 10 mm and length 1.0 m fixed at one end. The other end is twisted by angle of  $10^\circ$  by applying a torque. If the maximum shear strain in the rod is  $p \times 10^{-3}$ , then p is equal to \_\_\_\_ (round off to two decimal places).

**Key: (0.8726)**

**Sol:**  $D = 10\text{mm}$ ,  $\theta = 10^\circ$

$L = 1\text{m}$

$\phi = P \times 10^{-3}$

$L\phi = R\theta$

$$1 \times 100 \times P \times 10^{-3} = 5 \times 10 \times \frac{\pi}{180}$$

$$P = \frac{50\pi}{180} = 0.8726$$

21. Which one of the following welding methods provides the highest heat flux (W/mm<sup>2</sup>)?

- (A) Plasma arc welding (B) Tungsten inert gas welding  
(C) Oxy-acetylene gas welding (D) Laser beam welding

**Key: (D)**

**Sol:**

	Welding process	(W/cm <sup>2</sup> ) Heat density	Temp(°C)
1.	Gas welding	10 <sup>2</sup> – 10 <sup>3</sup>	2500-3500
2.	Shielded metal Arc welding	10 <sup>4</sup>	>6000
3.	Gas metal Arc welding	10 <sup>5</sup>	8000-10,000
4.	Plasma Arc welding	10 <sup>6</sup>	15000-30000
5.	Electron beam welding	10 <sup>7</sup> – 10 <sup>8</sup>	20000-30000
6.	Laser beam welding	10 <sup>9</sup>	>30,000

22. Water flows through a pipe with a velocity given by  $\vec{V} = \left(\frac{4}{t} + x + y\right)\hat{j}$  m/s, where  $\hat{j}$  is the unit vector in the y direction, t(>0) is in seconds, and x and y are in meters. The magnitude of total acceleration at the point (x, y) = (1, 1) at t = 2s is \_\_\_\_\_ m/s<sup>2</sup>.

**Key: (3)**

**Sol:**  $\vec{V} = \left(\frac{4}{t} + x + y\right)\hat{j}$  m/sec

$\vec{V} = u\hat{i} + v\hat{j} + w\hat{k}$

Acceleration at any point x, y, z and any time 't' is given as

$$a_{(x,y,z,t)} = \frac{d\vec{V}}{dt} + u \frac{d\vec{V}}{dx} + v \frac{d\vec{V}}{dy} + w \frac{d\vec{V}}{dz}$$

Given that x = 1, y = 1, t = 2, z = 0 and u = 0,  $V = \left(\frac{4}{t} + x + y\right)$ , w = 0

then,

$$\frac{d\vec{V}}{dt} = \frac{d}{dt} \left(\frac{4}{t} + x + y\right)\hat{j}, \hat{j} \cdot \hat{j} = -\frac{4}{t^2}$$

$$\frac{d\vec{V}}{dx} = \frac{d}{dx} \left(\frac{4}{t} + x + y\right)\hat{j}, \hat{j} \cdot \hat{j} = 1$$

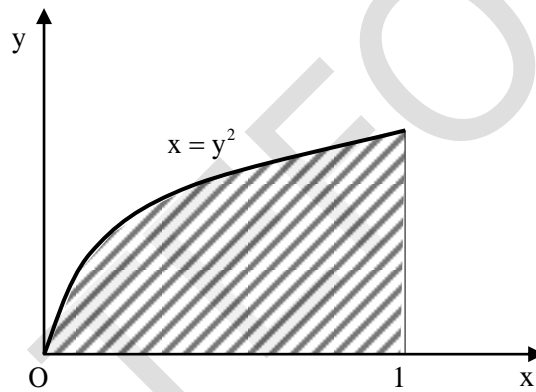


$$\frac{d\vec{V}}{dy} = \frac{d}{dy} \left( \frac{4}{t} + x + y \right) \mathbf{j}, \mathbf{j} = 1$$

$$\frac{d\vec{V}}{dz} = \frac{d}{dz} \left( \frac{4}{t} + x + y \right) \mathbf{j}, \mathbf{j} = 0$$

$$\begin{aligned} \therefore a_{(1,1,0,2)} &= \frac{-4}{t^2} + (0)(1) + \left( \frac{4}{t} + x + y \right) (1) + (0)(0) \\ &= \frac{-4}{t^2} + \frac{4}{t} + x + y \\ &= \frac{-4}{2^2} + \frac{4}{2} + 1 + 1 = -1 + 2 + 1 + 1 = 3 \text{ m/sec}^2 \end{aligned}$$

23. A parabola  $x = y^2$  with  $0 \leq x \leq 1$  is shown in the figure. The volume of the solid of rotation obtained by rotating the shaded area by  $360^\circ$  around the x-axis is

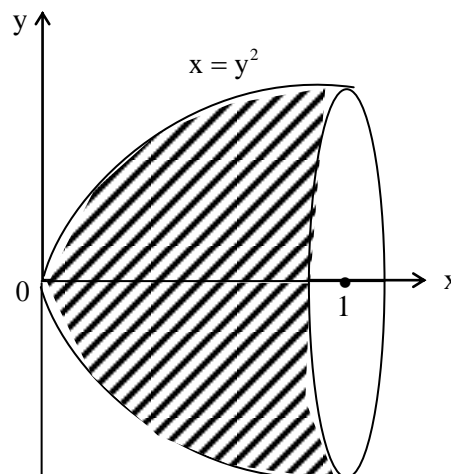


- (A)  $\frac{\pi}{4}$                       (B)  $\frac{\pi}{2}$                       (C)  $2\pi$                       (D)  $\pi$

**Key: (B)**

**Sol:** Volume of the solid of rotation obtained by rotating around the x – axis is given by

$$\begin{aligned} V &= \int_{x=a}^b \pi y^2 dx \\ \Rightarrow V &= \int_{x=0}^1 \pi x dx \quad [\because y^2 = x] \\ &= \pi \left[ \frac{x^2}{2} \right]_0^1 = \frac{\pi}{2} \end{aligned}$$



24. A spur gear with  $20^\circ$  full depth teeth is transmitting 20 kW at 200 rad/s. The pitch circle diameter of the gear is 100mm. The magnitude of the force applied on the gear in the radial direction is

- (A) 1.39 kN                      (B) 2.78 kN                      (C) 0.36 kN                      (D) 0.73 kN

**Key: (D)**

**Sol:**  $\phi = 20^\circ, P = 20\text{kW}, \omega = 200\text{rad/sec.}$

$$D = 100\text{mm}, F_R = ?$$

$$T = \frac{P}{\omega} = \frac{20 \times 10^3}{200} = 100\text{Nm}$$

$$F_t = \frac{T}{R} = \frac{100}{50 \times 10^{-3}} = 2000\text{N}$$

$$F_R = F_t \tan \phi = 2000 \tan 20^\circ = 727.9\text{N}$$

25. For the equation  $\frac{dy}{dx} + 7x^2y = 0$ , if  $y(0) = 3/7$ , then the value of  $y(1)$  is

- (A)  $\frac{7}{3}e^{-7/3}$                       (B)  $\frac{3}{7}e^{-7/3}$                       (C)  $\frac{3}{7}e^{-3/7}$                       (D)  $\frac{7}{3}e^{-3/7}$

**Key: (B)**

**Sol:** Given D.E is  $\frac{dy}{dx} + 7x^2y = 0, y(0) = 3/7$

The value of  $y(1)$  is \_\_\_\_\_.

$$\therefore \frac{dy}{dx} + 7x^2(y) = 0 \rightarrow (1)$$

$\therefore$  The equation (1) is linear D.E, Where  $P = 7x^2; Q = 0$

$$\text{I.F} = e^{\int P dx} = e^{\int 7x^2 dx} = e^{7(x^3/3)}$$

Solution of equation (1) is

$$y \cdot (\text{I.F}) = \int Q \cdot (\text{I.F}) dx + C$$

$$\Rightarrow ye^{\frac{7x^3}{3}} = \int 0 \cdot (\text{I.F}) dx + C \Rightarrow ye^{\frac{7x^3}{3}} = C$$

$$\Rightarrow y = C e^{-\frac{7x^3}{3}} \rightarrow (2)$$

Given  $y = 3/7$  at  $x = 0$

$$\therefore (2) \Rightarrow 3/7 = C$$

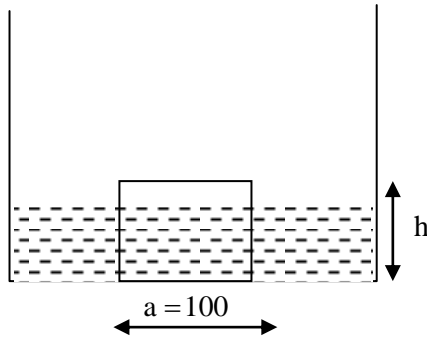
$$\text{From (2), } y = \frac{3}{7} e^{-\frac{7}{3}x^3} \Rightarrow y(1) = \frac{3}{7} e^{-7/3}$$

**Q. No. 26 to 55 Carry Two Marks Each**

26. A cube of side 100 mm is placed at the bottom of an empty container on one of its faces. The density of the material of the cube is  $800 \text{ kg/m}^3$ . Liquid of density  $1000 \text{ kg/m}^3$  is now poured into the container. The minimum height to which the liquid needs to be poured into the container for the cube to just lift up is \_\_\_\_\_ mm.

**Key: (80)**

**Sol:**



Given that density of cube material  $e_{\text{cube}} = 800 \text{ kg/m}^3$

Density of liquid poured  $e_{\text{water}} = 1000 \text{ kg/m}^3$

Weight of cube  $= e_{\text{cube}} \times \text{volume of cube} \times g$

$$= 800 \times 0.1 \times 0.1 \times 0.1 \times g = 0.8g \text{ N}$$

To just lift the cube, weight of cube = buoyancy force  
buoyancy force = weight of liquid displaced

$$= e_{\text{liquid}} \times \text{volume of liquid} \times g = 1000 \times 0.1 \times 0.1 \times h \times g = 10hg$$

Where  $h$  = height of water poured

By equating weight of cube = buoyancy force

$$0.8g = 10hg$$

$$h = \frac{0.8}{10} = 0.08 \text{ m} = 80 \text{ mm}$$

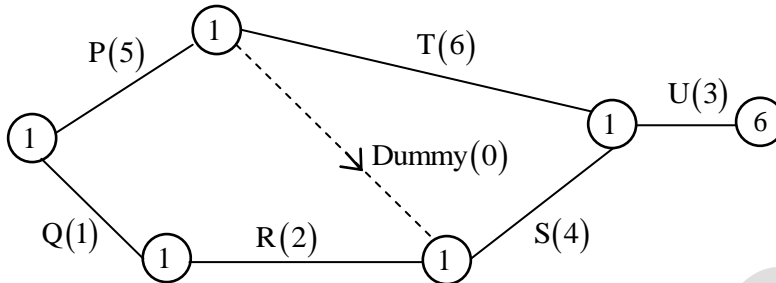
27. A project consists of six activities. The immediate predecessor of each activity and the estimated duration is also provided in the table below:

Activity	Immediate predecessor	Estimated duration (weeks)
P	-	5
Q	-	1
R	Q	2
S	P, R	4
T	P	6
U	S, T	3

If all activities other than S take the estimated amount of time, the maximum duration (in weeks) of the activity S without delaying the completion of the project is \_\_\_\_\_.

**Key: (6)**

**Sol:** From the given data, we can represent network flow as follows



Considering path 1-2-5-6, time taken will be = 5+ 6+ 3= 14 weeks

Considering path 1-2-4-5-6, time taken will be=5+0+4+5=12 weeks.

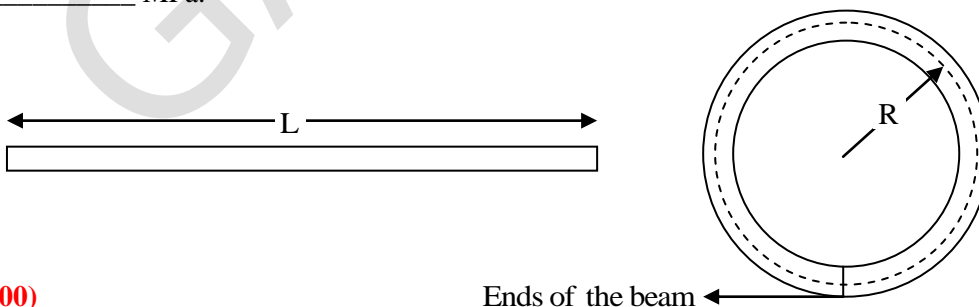
Considering path 1-3-4-5-6, time taken will be = 1+2+4+3 =10 weeks

Maximum time taken is 14 weeks, so '2' weeks can be delayed so that 1-2-4-5-6 path will also take 14 weeks.

So answer is 4 weeks +2 weeks = 6 weeks

Duration can be given for activities without delay the project.

28. Consider an elastic straight beam of length  $L = 10\pi$  m, with square cross-section of side  $a = 5$  mm, and Young's modulus  $E = 200$  GPa. This straight beam was bent in such a way that the two ends meet, to form a circle of mean radius  $R$ . Assuming that Euler-Bernoulli beam theory is applicable to this bending problem, the maximum tensile bending stress in the bent beam is \_\_\_\_\_ MPa.



**Key: (100)**

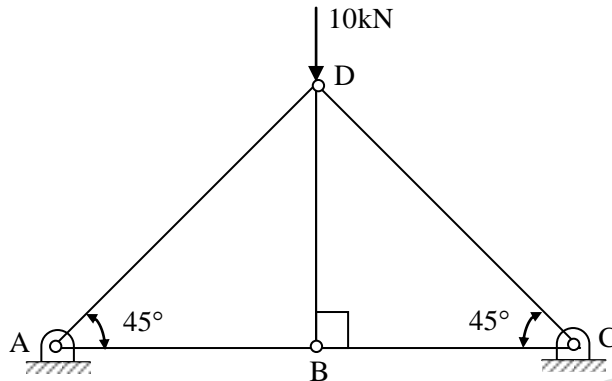
**Sol:**  $L = 10\pi$  mts;  $a = 5$  mm,  $E = 200$  GPa

$$L = 2\pi R$$

$$R = \frac{10\pi}{2\pi} = 5\text{mts} = 5000\text{mm.}$$

$$\sigma = \frac{E}{R} y = \frac{200 \times 10^3}{5000} \times \left(\frac{5}{2}\right) = 100\text{MPa}$$

29. A truss is composed of members AB, BC, CD, AD and BD, as shown in the figure. A vertical load of 10 kN is applied at point D. The magnitude of force (in kN) in the member BC is \_\_\_\_\_.

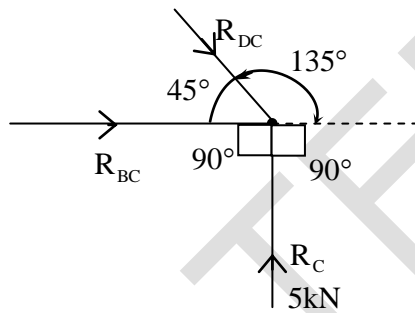


**Key: (5)**

**Sol:** Due symmetry

$$R_A = R_C = \frac{10\text{kN}}{2} = 5\text{kN}$$

Joint C



$$\frac{R_{BC}}{\sin 225^\circ} = \frac{R_{DC}}{\sin 90^\circ} = \frac{5}{\sin 45^\circ}$$

$$R_{BC} = \frac{5 \sin 225}{\sin 45} = -5\text{kN (Tension)}$$

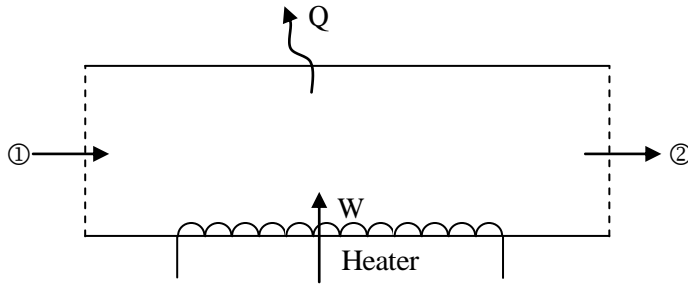
30. A gas is heated in a duct as it flows over a resistance heater. Consider a 101 kW electric heating system. The gas enters the heating section of the duct at 100 kPa and 27°C with a volume flow rate of 15m<sup>3</sup>/s. If heat is lost from the gas in the duct to the surroundings at a rate of 51kW, the exit temperature of the gas is

(Assume constant pressure, ideal gas, negligible change in kinetic and potential energies and constant specific heat;  $C_p = 1 \text{ kJ/kg.K}$ ;  $R = 0.5 \text{ kJ/kg.K}$ ).

- (A) 53°C                      (B) 32°C                      (C) 37°C                      (D) 76°C

**Key: (B)**

**Sol:**



**Inlet conditions**

$$P_1 = 100 \text{ kPa}, T_1 = 27^\circ\text{C} = 300 \text{ K}$$

$$V_1 = V_2 = 15 \text{ m}^3/\text{s}$$

$$Q = -51 \text{ kW}$$

$$W = -101 \text{ kW}$$

$$\text{Now, mass flow rate } \dot{m} = \frac{P_1 V_1}{RT_1}$$

$$\dot{m} = \frac{100 \times 15}{0.5 \times 300} = 10 \text{ kg/s}$$

From 1<sup>st</sup> law of thermodynamics and steady flow energy equation

$$Q = \dot{m}(h_2 - h_1) + W$$

$$-51 = \dot{m}(h_2 - h_1) - 101$$

$$\dot{m}(h_2 - h_1) = 50$$

$$10(h_2 - h_1) = 50 \Rightarrow h_2 - h_1 = 5$$

$$C_p(T_2 - T_1) = 5 \Rightarrow T_2 = 27 + 5 = 32^\circ\text{C}$$

**31.** A harmonic function is analytic if it satisfies the Laplace equation. If  $u(x, y) = 2x^2 - 2y^2 + 4xy$  is a harmonic function, then its conjugate harmonic function  $v(x, y)$  is

(A)  $-4xy + 2y^2 - 2x^2 + \text{constant}$

(B)  $4xy - 2x^2 + 2y^2 + \text{constant}$

(C)  $2x^2 - 2y^2 + xy + \text{constant}$

(D)  $4y^2 - 4xy + \text{constant}$

**Key: (B)**

**Sol:** Given,  $u(x, y) = 2x^2 - 2y^2 + 4xy$  is a harmonic function.

$$\Rightarrow \frac{\partial u}{\partial x} = 4x + 4y; \frac{\partial u}{\partial y} = -4y + 4x$$

The conjugate harmonic function  $v(x, y)$  is obtained as follows:

$$dv = \frac{\partial v}{\partial x} dx + \frac{\partial v}{\partial y} dy \left[ \because \text{from total differential of } v(x, y) \right]$$

$$\Rightarrow dv = \left( -\frac{\partial u}{\partial y} \right) dx + \left( \frac{\partial u}{\partial x} \right) dy \quad , \text{ using C-R equations}$$

$$\Rightarrow dv = -[-4y + 4x] dx + (4x + 4y) dy$$

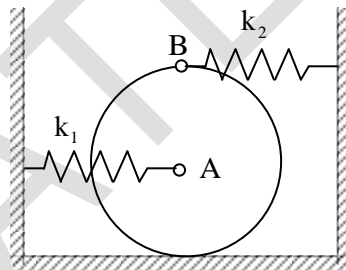
Exact D.E

$$\Rightarrow \int dv = -\int (-4y + 4x) dx + \int (4x + 4y) dy$$

$$\Rightarrow v(x, y) = -\left[ -4yx + 4\left(\frac{x^2}{2}\right) \right] + 4\left[\frac{y^2}{2}\right] + C$$

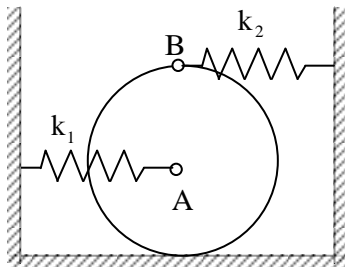
$$\Rightarrow v(x, y) = 4xy - 2x^2 + 2y^2 + C$$

32. A uniform thin disk of mass 1 kg and radius 0.1 m is kept on a surface as shown in the figure. A spring of stiffness  $k_1 = 400 \text{ N/m}$  is connected to the disk center A and another spring of stiffness  $k_2 = 100 \text{ N/m}$  is connected at point B just above point A on the circumference of the disk. Initially, both the springs are unstretched. Assume pure rolling of the disk. For small disturbance from the equilibrium, the natural frequency of vibration of the system is \_\_\_\_\_ rad/s (round off to one decimal place).

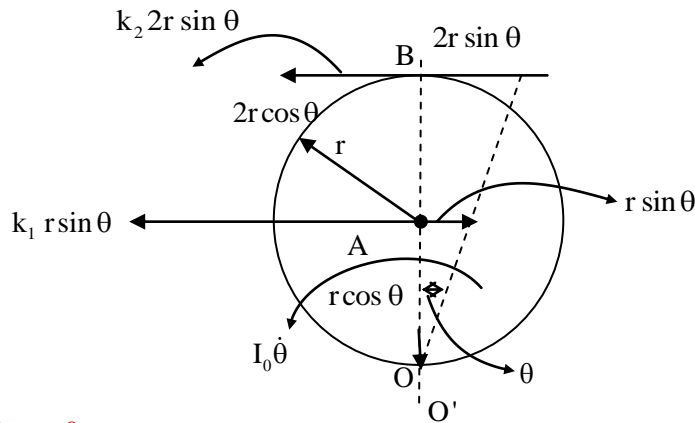


**Key: (23.1)**

**Sol:**



Give a small displacement to Disc about 'O'



$$\Sigma m_0 = 0$$

$$I_0 \ddot{\theta} + (k_1 r \sin \theta)(r \cos \theta) + (k_2 2r \sin \theta)(2r \cos \theta) = 0$$

$$I_0 = I_{C.G.} + mr^2 = \frac{mr^2}{2} + mr^2 = \frac{3}{2}mr^2 = \frac{3}{2} \times 1 \times 0.1^2 = 0.015 \text{ kg m}^2$$

$$m = 1 \text{ kg}, r = 0.1 \text{ m}, k_1 = 400 \text{ N/m}, k_2 = 100 \text{ N/m}$$

$$\text{Assume } \sin \theta \cong \theta, \cos \theta = 1$$

$$0.015 \ddot{\theta} + (400)(0.1)^2 \theta + (100)(2)(0.1)(\theta)(2)(0.1) = 0$$

$$0.015 \ddot{\theta} + 8\theta = 0$$

$$\omega_n = \sqrt{\frac{8}{0.015}} = 23.09 \cong 23.1 \text{ rad/sec}$$

33. In ASA system, the side cutting and end cutting edge angles of a sharp turning tool are  $45^\circ$  and  $10^\circ$ , respectively. The feed during cylindrical turning is  $0.1 \text{ mm/rev}$ . The center line average surface roughness (in  $\mu\text{m}$ , round off to one decimal place) of the generated surface is \_\_\_\_\_.

**Key: (3.747)**

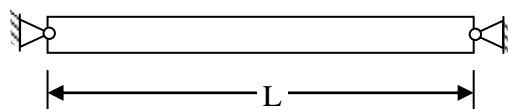
**Sol:** Given,  $C_s = 45^\circ$ ,  $C_e = 10^\circ$

$$f = 0.1 \text{ mm / rev}$$

$$R_a \text{ or CLA} = \frac{f}{4(\tan C_s + \cot C_e)}$$

$$= \frac{0.1}{4(\tan 45^\circ + \cot 10^\circ)} = 3.747 \times 10^{-3} \text{ mm} = 3.747 \mu\text{m}.$$

34. Consider a prismatic straight beam of length  $L = \pi \text{ m}$ , pinned at the two ends as shown in the figure.





The beam has a square cross-section of side  $p = 6\text{mm}$ . The Young's modulus  $E = 200\text{GPa}$ , and the coefficient of thermal expansion  $\alpha = 3 \times 10^{-6}\text{K}^{-1}$ . The minimum temperature rise required to cause Euler buckling of the beam is \_\_\_\_\_ K.

**Key: (1)**

**Sol:**  $L = \pi, \Delta T = ?$

$$\text{Area} = 6 \times 6 = 36\text{mm}^2, I = \frac{6^4}{12} = 108\text{mm}^4$$

$$E = 200\text{GPa}$$

$$\alpha = 3 \times 10^{-6}\text{K}^{-1}$$

$$P_E = \frac{\pi^2 EI}{l_c^2} = \frac{\pi^2 \times 200 \times 10^3 \times 108}{\pi^2 \times 10^6} = 21.6\text{MN}$$

$$P_E = EA\alpha\Delta T$$

$$21.6 = 200 \times 10^3 \times 36 \times 3 \times 10^{-6} \times \Delta T$$

$$\Delta T = 1\text{K}.$$

35. The set of equations

$$x + y + z = 1$$

$$ax - ay + 3z = 5$$

$$5x - 3y + az = 6$$

has infinite solutions, if a =

(A) 4

(B) -4

(C) -3

(D) 3

**Key: (A)**

**Sol:** 
$$\left. \begin{array}{l} x + y + z = 1 \\ ax - ay + 3z = 5 \\ 5x - 3y + az = 6 \end{array} \right\} \rightarrow [\text{Non-homogeneous}]$$

$$\text{Augmented matrix, } [A|B] = \left[ \begin{array}{ccc|c} 1 & 1 & 1 & 1 \\ a & -a & 3 & 5 \\ 5 & -3 & a & 6 \end{array} \right]$$

$$R_2 \leftrightarrow R_3$$

$$[A|B] \sim \left[ \begin{array}{ccc|c} 1 & 1 & 1 & 1 \\ 5 & -3 & a & 6 \\ a & -a & 3 & 5 \end{array} \right]$$

$$\text{Applying } R_2 \rightarrow R_2 - 5R_1; R_3 \rightarrow R_3 - aR_1$$

$$\sim \left[ \begin{array}{ccc|c} 1 & 1 & 1 & 1 \\ 0 & -8 & a-5 & 1 \\ 0 & -2a & 3-a & 5-a \end{array} \right]$$

$$R_3 \rightarrow 4R_3 - aR_2$$

$$\sim \left[ \begin{array}{ccc|c} 1 & 1 & 1 & 1 \\ 0 & -8 & a-5 & 1 \\ 0 & 0 & -a^2+a+12 & 20-5a \end{array} \right]$$

To have infinite number of solutions,

$$-a^2 + a + 12 = 0 \quad \& \quad 20 - 5a = 0$$

$$\Rightarrow (a-4)(a+3) = 0 \quad \Rightarrow a = 4$$

$$\Rightarrow a = 4 \text{ (or) } a = -3 \quad \& \quad a = 4$$

$\therefore$  a must be equal to '4' only.

36. In a UTM experiment, a sample of length 100 mm, was loaded in tension until failure. The failure load was 40 kN. The displacement, measured using the cross-head motion, at failure, was 15 mm. The compliance of the UTM is constant and is given by  $5 \times 10^{-8}$  m/N. The strain at failure in the sample is \_\_\_\_\_%.

**Key: (2)**

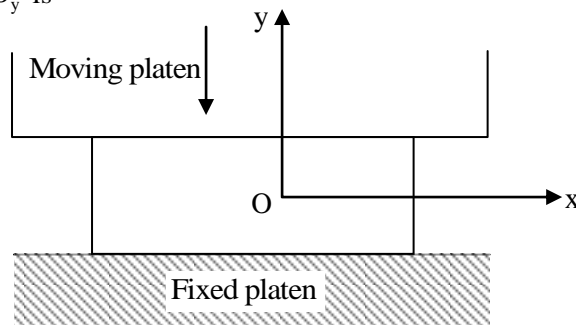
**Sol:** Compliance ( $\epsilon$ ) =  $\frac{\delta l}{P} = 5 \times 10^{-8}$  m/N,  $P = 40$ KN,  $L = 100$ mm

$$\epsilon = \frac{\sigma}{E} = \frac{P}{AE}; \quad C = \frac{\delta L}{P} = \frac{L}{AE} = 5 \times 10^{-8}$$

$$\delta l = 40 \times 10^3 \times 5 \times 10^{-8} = 2 \times 10^{-3} \text{ mts} = 2 \text{ mm}$$

$$\epsilon = \frac{\delta l}{l} = \frac{2}{100} = 0.02 \text{ or } 2\%$$

37. A plane-strain compression (forging) of a block is shown in the figure. The strain in the z-direction is zero. The yield strength ( $S_y$ ) in uniaxial tension/compression of the material of the block is 300 MPa and it follows the Tresca (maximum shear stress) criterion. Assume that the entire block has started yielding. At a point where  $\sigma_x = 40$  MPa (compressive) and  $\tau_{xy} = 0$ , the stress component  $\sigma_y$  is



- (A) 260 MPa (tensile) (B) 340 MPa (compressive)  
(C) 260 MPa (compressive) (D) 340 MPa (tensile)

**Key: (B)**

**Sol:**  $\sigma_y = 300\text{MPa}$ ,  $\sigma_x = 40\text{MPa}$  (compressive),  $\tau_{xy} = 0$ ,  $\sigma_z = ?$

For plane strain

$$\epsilon_z = 0 \Rightarrow \frac{\sigma_z}{E} - \nu \frac{\sigma_x}{E} - \nu \frac{\sigma_y}{E} = 0 \Rightarrow \sigma_z = \nu(\sigma_x + \sigma_y)$$

$$\sigma_z = \nu(-40 + \sigma_y)$$

$$\tau_{\max} = \text{Max} \left[ \left| \frac{\sigma_x - \sigma_y}{2} \right|, \left| \frac{\sigma_y - \sigma_z}{2} \right|, \left| \frac{\sigma_z - \sigma_x}{2} \right| \right]$$

$$\tau_{\max} = \frac{S_y}{2 \times \text{F.S.}} = \text{Max} \left[ \left| \frac{-40 - \sigma_y}{2} \right|, \left| \frac{\sigma_y - \nu(\sigma_y - 40)}{2} \right|, \left| \frac{\nu(\sigma_y - 40) + 40}{2} \right| \right]$$

From the above equation Maximum will be the first one i.e.,  $\left| \frac{-40 - \sigma_y}{2} \right| \leq \frac{S_y}{2 \times \text{F.S.}}$

$$\frac{-40 - \sigma_y}{2} = \frac{+S_y}{2 \times \text{F.S.}} \quad \text{or} \quad \frac{-40 - \sigma_y}{2} = \frac{-S_y}{2 \times \text{F.S.}}$$

$$-40 - \sigma_y = 300$$

$$-40 - \sigma_y = -300$$

$$\sigma_y = -340\text{MPa}$$

$$\sigma_y = 260\text{MPa}$$

$$\sigma_y = 340\text{MPa (Compressive)} \quad \text{or} \quad \sigma_y = 260\text{MPa (Tensile)}$$

$$40 + \sigma_y = 300 \Rightarrow \sigma_y = 260 \text{ MPa (Tension)}$$

But in the forging operation  $\sigma_y$  can't be tensile hence the answer is 340MPa (compressive).

38. Match the following sand mold casting defects with their respective causes.

Defect	Cause
(P) Blow hole	1. Poor collapsibility
(Q) Misrun	2. Mold erosion
(R) Hot tearing	3. Poor permeability
(S) Wash	4. Insufficient fluidity

Codes:

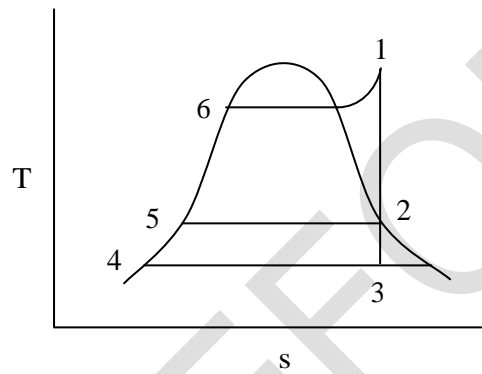
- (A) P-3, Q-4, R-2, S-1 (B) P-4, Q-3, R-1, S-2  
(C) P-2, Q-4, R-1, S-3 (D) P-3, Q-4, R-1, S-2

**Key: (D)**

39. A steam power cycle with regeneration as shown below on the T-s diagram employs a single open feedwater heater for efficiency improvement. The fluids mix with each other in an open feedwater heater. The turbine is isentropic and the input (bleed) to the feedwater heater from the turbine is at state 2 as shown in the figure. Process 3-4 occurs in the condenser. The pump work is negligible. The input to the boiler is at state 5.

The following information is available from the steam tables:

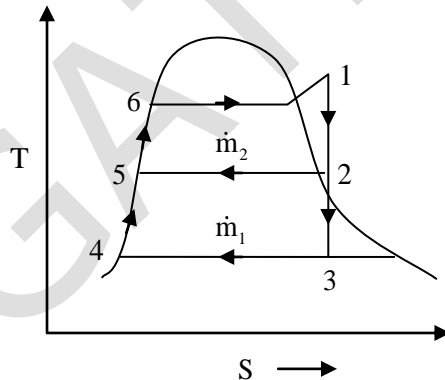
State	1	2	3	4	5	6
Enthalpy (kJ/kg)	3350	2800	2300	175	700	1000



The mass flow rate of steam bled from the turbine as a percentage of the total mass flow rate at the inlet to the turbine at state 1 is \_\_\_\_\_.

**Key: (20)**

**Sol:**



Let  $\dot{m}_2$  mass is bled at state 2 and  $\dot{m}_1$  mass goes to the condenser.

Assuming no heat loss from the feed water heater,

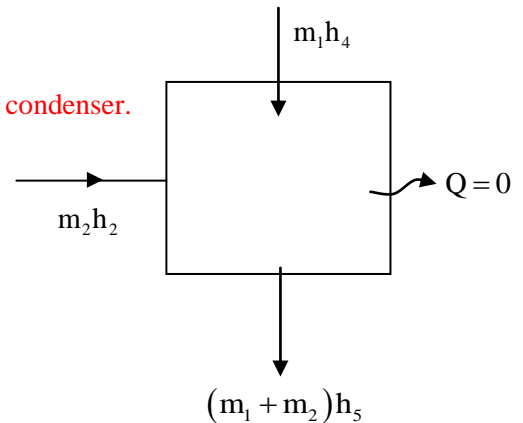
$$m_1 h_4 + m_2 h_2 = (m_1 + m_2) h_5 \rightarrow (1)$$

$$h_4 = 175 \text{ kJ/kg}, h_2 = 2800 \text{ kJ/kg}, h_5 = 700 \text{ kJ/kg}$$

$$\therefore 175 m_1 + 2800 m_2 = (m_1 + m_2) 700$$

$$\therefore 2100 m_2 = 525 m_1$$

$$\frac{m_2}{m_1} = 0.25 \Rightarrow \frac{m_2}{m_1 + m_2} = 0.2. \text{ Hence } 20\%$$



40. The rotor of turbojet engine of an aircraft has a mass 180 kg and polar moment of inertia  $10 \text{ kg.m}^2$  about the rotor axis. The rotor rotates at a constant speed of 1100 rad/s in the clockwise direction when viewed from the front of the aircraft. The aircraft while flying at a speed of 800 km per hour takes a turn with a radius of 1.5 km to the left. The gyroscopic moment exerted by the rotor on the aircraft structure and the direction of motion of the nose when the aircraft turns, are
- (A) 1629.6 N.m and the nose goes up  
 (B) 1629.6 N.m and the nose goes down  
 (C) 162.9 N.m and the nose goes down  
 (D) 162.9 N.m and the nose goes up

**Key: (B)**

**Sol:**  $m = 180 \text{ kg}$   $\omega = 1100 \text{ rad/sec}$ ,  $V = 800 \text{ kmph}$   $R = 1.5 \text{ mts}$

$$I = 10 \text{ kg} - \text{m}^2$$

$$\omega_p = \frac{V}{R} = \frac{800 \times \frac{5}{18}}{1.5 \times 1000} = 0.148 \text{ rad/sec}$$

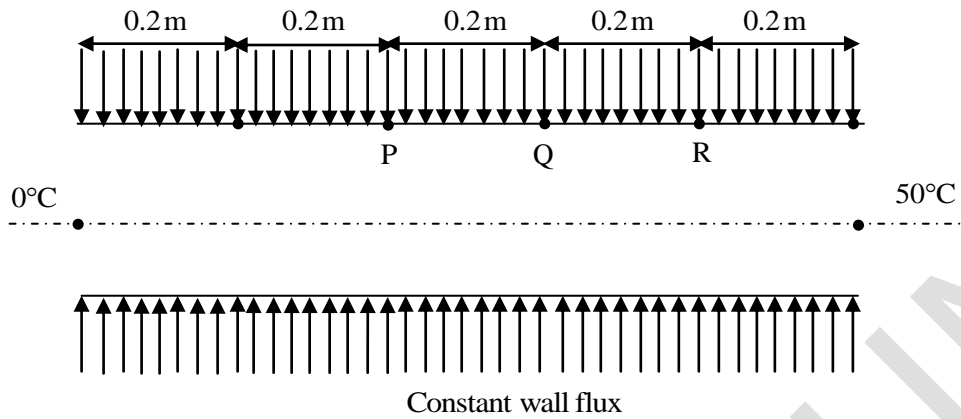
$$C = I\omega\omega_p = 1100 \times 10 \times 148.148 = 1629.628 \text{ Nm}$$



Dip the nose and Raise the tail. So answer is option 'B'.

41. The wall of a constant diameter pipe of length 1 m is heated uniformly with flux  $q''$  by wrapping a heater coil around it. The flow at the inlet to the pipe is hydrodynamically fully developed. The fluid is incompressible and the flow is assumed to be laminar and steady all through the pipe. The bulk temperature of the fluid is equal to  $0^\circ\text{C}$  at the inlet and  $50^\circ\text{C}$  at the exit. The wall temperatures are measured at three locations, P, Q and R, as shown in the figure. The flow thermally develops after some distance from the inlet. The following measurements are made:

Point	P	Q	R
Wall Temp ( $^\circ\text{C}$ )	50	80	90

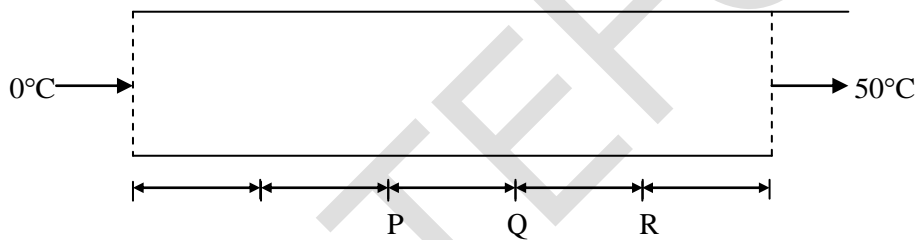


Among the locations P, Q and R, the flow is thermally developed at:

- (A) P and Q only      (B) P, Q and R      (C) R only      (D) Q and R only

**Key: (D)**

**Sol:**



From heat balance

$$q'' \times \pi d \times x = m.c. (T_B - T_{in}) \quad \text{---(1)}$$

Where  $m.c.$  = heat capacity of fluid and

$$T_B = \text{bulk mean temperature} \quad \therefore T_B = \left( \frac{q'' \pi d}{m.c.} \right) x + T_{in}$$

At inlet  $z = 0, T_{in} = 0$

$$x = 1m, T_B = 50^\circ C$$

$$\therefore \frac{q'' \times \pi d}{m.c.} = Z(\text{constant}) = 50$$

$$\therefore \boxed{T_B = 50x} \quad \text{---(ii)}$$

Now :  $q'' \times \pi d = h^* (T_w - T_B)$  (At any section)

$$\therefore \frac{q'' \pi d}{h^*} = (T_w - T_B)$$

$$\therefore \frac{q'' \pi d}{h^*} + T_B = T_w$$

$$\therefore T_w = C + T_B \quad \left[ C = \frac{q'' \pi d}{h^*} \right] \rightarrow \text{constant for fully developed flow.}$$

$$T_w = C + 50x.$$

At P,  $T_w = 50^\circ\text{C}$ ,  $x = 0.4$

$$\therefore 50 - 50 \times 0.4 = C = 30$$

At Q,  $T_w = 80^\circ\text{C}$ ,  $x = 0.6$

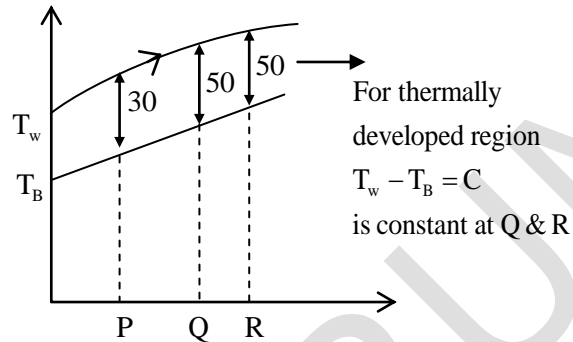
$$\therefore 80 - 50 \times 0.6 = 50 = C$$

At R,  $T_w = 90^\circ$ ,  $x = 0.8$

$$90 - 50 \times 0.8 = 50 = C$$

$\therefore$  Clearly we see that  $T_w - T_B$  is constant from Q

$\therefore$  Flow will be thermally developed between Q & R



42. At a critical point in a component, the state of stress is given as  $\sigma_{xx} = 100 \text{ MPa}$ ,  $\sigma_{yy} = 220 \text{ MPa}$ ,  $\sigma_{xy} = \sigma_{yx} = 80 \text{ MPa}$  and all other stress components are zero. The yield strength of the material is 468 MPa. The factor of safety on the basis of maximum shear stress theory is \_\_\_\_\_ (round off to one decimal place).

**Key: (1.8)**

**Sol:**  $\sigma_{xx} = 100 \text{ MPa}$ ,  $\sigma_{yy} = 220 \text{ MPa}$ ,  $\sigma_{xy} = \sigma_{yx} = 80 \text{ MPa}$ ,  $\sigma_{yt} = 468 \text{ MPa}$ .

$$\frac{\tau_{yt}}{\text{F.O.S}} = \frac{\sigma_{yt}}{2 \text{F.O.S}} = \left[ \frac{\sigma_1 - \sigma_2}{2}, \frac{\sigma_1}{2}, \frac{\sigma_2}{2} \right]$$

$$\sigma_{1,2} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left( \frac{\sigma_x - \sigma_y}{2} \right)^2 + \tau_{xy}^2}$$

$$= \frac{100 + 220}{2} \pm \sqrt{\left( \frac{100 - 220}{2} \right)^2 + 80^2}$$

$$= 160 \pm 100 = 260 \text{ MPa}, 60 \text{ MPa}$$

$$\frac{\sigma_{yt}}{2 \times \text{F.O.S}} = \text{Max} \left[ \frac{260 - 60}{2}, \frac{260}{2}, \frac{60}{2} \right]$$

$$\text{F.O.S} = \frac{468}{260} = 1.8$$

43. A gas turbine with air as the working fluid has an isentropic efficiency of 0.70 when operating at a pressure ratio of 3. Now, the pressure ratio of the turbine is increased to 5, while maintaining the same inlet conditions. Assume air as a perfect gas with specific heat ratio  $\gamma = 1.4$ . If the specific work output remains the same for both the cases, the isentropic efficiency of the turbine at the pressure ratio of 5 is \_\_\_\_\_ (round off to two decimal places).

**Key: (0.51)**

**Sol:**  $\frac{P_1}{P_2} = 3, \frac{P_1}{P_3} = 5, r_p = \text{pressure ratio}$

Work done by turbine 1 for  $r_p = 3$

$$W_{1-2'} = mc_p (T_1 - T_2) = mc_p \times \eta_{1-2'} \times (T_1 - T_2)$$

$$= m \times c_p \times \eta_{1-2'} \times \left[ T_1 - \frac{T_1}{\left(r_{p1}\right)^{\frac{\gamma-1}{\gamma}}} \right]$$

$$W_{1-2'} = \left[ m \times c_p \times T_1 \right] \times \eta_{1-2'} \left[ 1 - \frac{1}{r_{p1}^{\frac{\gamma}{\gamma-1}}} \right] \quad \text{---(i)}$$

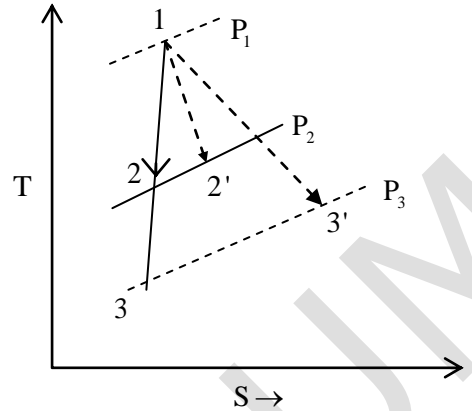
Since  $W_{1-2'} = W_{1-3'}$

$$\therefore \eta_{1-3'} \left[ 1 - \frac{1}{\left(r_{p2}\right)^{\frac{\gamma}{\gamma-1}}} \right] = \eta_{1-2'} \left[ 1 - \frac{1}{r_{p1}^{\frac{\gamma}{\gamma-1}}} \right]$$

Putting  $\eta_{1-2'} = 0.7, r_{p1} = 3, r_{p2} = 5$

$$\therefore \eta_{1-3'} = 0.5115 \Rightarrow \eta_{1-3'} \approx 51.15\%$$

Hence efficiency = 0.5115



44. The value of the following definite integral is \_\_\_\_\_ (round off to three decimal places)

$$\int_1^e (x \ln x) dx$$

**Key: (2.097)**

**Sol:**  $\int_1^e (x \ln x) dx$

Let  $\ln x = t \Rightarrow x = e^t \Rightarrow dx = e^t dt$

If  $x = 1 \Rightarrow t = 0$

If  $x = e \Rightarrow t = \ln e = 1$

$$\therefore \int_1^e x \ln x dx = \int_0^1 e^t te^t dt = \int_0^1 te^{2t} dt$$

$$= \left[ t \left[ \frac{e^{2t}}{2} \right] - \left[ \frac{e^{2t}}{4} \right] \right]_0^1 = \left[ \frac{e^2}{2} - \frac{e^2}{4} \right] - \left[ 0 - \frac{1}{4} \right] = e^2 \left[ \frac{1}{2} - \frac{1}{4} \right] + \frac{1}{4} = 2.097.$$



45. Taylor's tool life equation is given by  $VT^n = C$ , where  $V$  is in m/min and  $T$  is in min. In a turning operation, two tools X and Y are used. For tool X,  $n = 0.3$  and  $C = 60$  and for tool Y,  $n = 0.6$  and  $C = 90$ . Both the tools will have the same tool life for the cutting speed (in m/min, round off to one decimal place) of \_\_\_\_\_.

**Key: (40.5)**

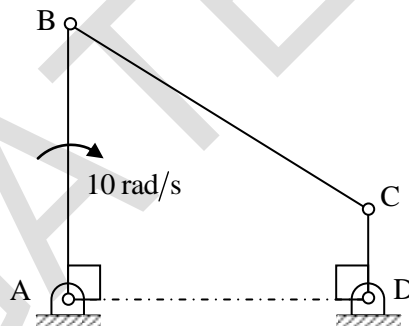
**Sol:**

Tool - X	Tool - Y
$n = 0.3$	$n = 0.6$
$C = 60$	$C = 90$
$VT_X^{0.3} = 60$	$VT_Y^{0.6} = 90$
$T_X = \left(\frac{60}{V_X}\right)^{1/0.3}$	$T_Y = \left(\frac{90}{V_Y}\right)^{1/0.6}$

For same toll life at breakeven ( $V_X = V_Y = V$ )

$$T_X = T_Y \left(\frac{60}{V_X}\right)^{10/6} = \left(\frac{90}{V_Y}\right)^{10/6} \therefore V = 40.5 \text{ m/min}$$

46. In a four bar planar mechanism shown in the figure,  $AB = 5$  cm,  $AD = 4$  cm and  $DC = 2$  cm. In the configuration shown, both  $AB$  and  $DC$  are perpendicular to  $AD$ . The bar  $AB$  rotates with an angular velocity of  $10$  rad/s. The magnitude of angular velocity (in rad/s) of bar  $DC$  at this instant is

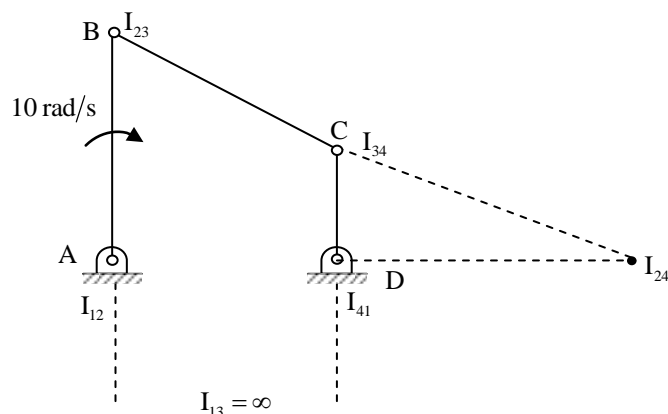


- (A) 25                      (B) 15                      (C) 10                      (D) 0

**Key: (A)**

**Sol:**

$AB = 5$  cm  
 $AD = 4$  cm and  $DC = 2$  cm,  
 $\omega_{AB} = 10$  rad/sec,  $\omega_{DC} = ?$   
 $I_{13} = \infty$  so the velocity of link  
 $BC$  is zero and now  $V_B = V_C$   
 $r_{AB} \cdot \omega_{AB} = r_{CD} \cdot \omega_{CD}$   
 $5 \times 10 = 2 \times \omega_{CD}$   
 $\omega_{CD} = 25$  rad/sec



47. If one mole of  $H_2$  gas occupies a rigid container with a capacity of 1000 liters and the temperature is raised from  $27^\circ C$  to  $37^\circ C$ , the change in pressure of the contained gas (round off to two decimal places), assuming ideal gas behavior, is \_\_\_\_\_ Pa. ( $R = 8.314 \text{ J/mol.K}$ ).

**Key: (83.14)**

**Sol:** Initially  $T_1 = 27^\circ C = 300K$   
 $n_1 = 1 \text{ mole}$   
 $\bar{R} = 8.314 \text{ KJ/mol-K}$

$$V_1 = 1000 \text{ litres} = 1m^3$$

$$\text{Finally, } T_2 = 37^\circ C = 310K$$

$$P_2 = ?$$

From ideal Gas relation

$$P_1 V_1 = (n\bar{R})T_1$$

$$P_1 = 8.314 \times 300 \text{ pascal}$$

$$P_1 = 300R$$

Now since the volume of container is constant hence.

$$V_1 = V_2$$

$$(\pi\bar{R}) \frac{T_1}{P_1} = (n\bar{R}) \frac{T_2}{P_2}$$

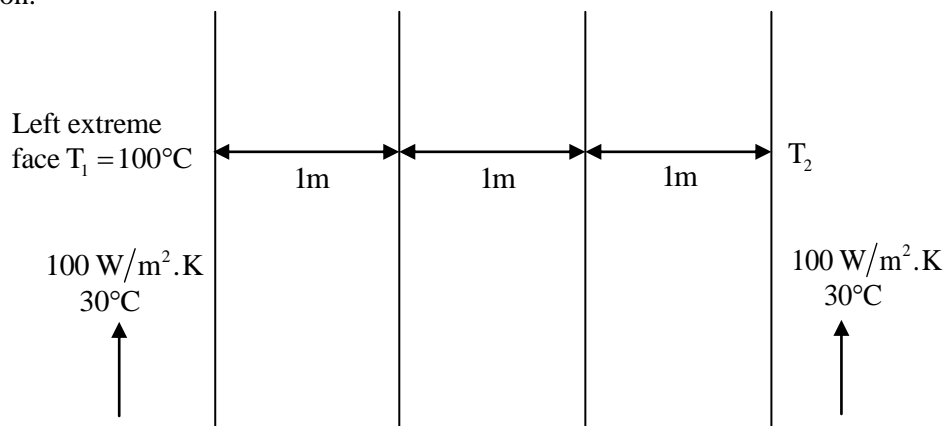
$$P_2 = P_1 \frac{T_2}{T_1} = 300R \times \frac{310}{300}$$

$$\therefore P_2 = 310\bar{R} \text{ (Pascal)}$$

$$\therefore \text{Change in pressure, } (P_2 - P_1) = (310 - 300)\bar{R} = 10\bar{R} = 10 \times 8.314$$

$$\Delta P = 83.14 \text{ pascal}$$

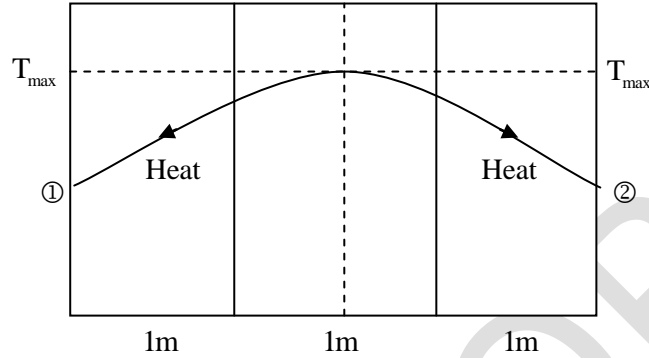
48. Three slabs are joined together as shown in the figure. There is no thermal contact resistance at the interfaces. The center slab experience a non-uniform internal heat generation with an average value equal to  $10000 \text{ Wm}^{-3}$ , while the left and right slabs have no internal heat generation.



All slabs have thickness equal to 1 m and thermal conductivity of each slab is equal to  $5 \text{ Wm}^{-1} \text{ K}^{-1}$ . The two extreme faces are exposed to fluid with heat transfer coefficient  $100 \text{ Wm}^{-2}\text{K}^{-1}$  and bulk temperature  $30^\circ\text{C}$  as shown. The heat transfer in the slabs is assumed to be one dimensional and steady, and all properties are constant. If the left extreme face temperature  $T_1$  is measured to be  $100^\circ\text{C}$ , the right extreme faced temperature  $T_2$  is \_\_\_\_\_  $^\circ\text{C}$ .

**Key: (100)**

**Sol:**



Since both sides conditions are same and heat is generated only in central plate

Hence both sides temperatures  $T_1$  &  $T_2$  will be equal

$$T_1 = T_2 = 100^\circ\text{C}$$

49. Five jobs ( $J_1, J_2, J_3, J_4$  and  $J_5$ ) need to be processed in a factory. Each job can be assigned to any of the five different machines ( $M_1, M_2, M_3, M_4$  and  $M_5$ ). The time duration taken (in minutes) by the machines for each of the jobs, are given in the table. However, each job is assigned to a specific machine in such a way that the total processing time is minimum. The total processing time is \_\_\_\_\_ minutes.

	$M_1$	$M_2$	$M_3$	$M_4$	$M_5$
$J_1$	40	30	50	50	58
$J_2$	269	38	60	26	38
$J_3$	40	34	28	24	30
$J_4$	28	40	40	32	48
$J_5$	28	32	38	22	44

**Key: (146)**

**Sol:** This problem can be solved by assignment problem

	M <sub>1</sub>	M <sub>2</sub>	M <sub>3</sub>	M <sub>4</sub>	M <sub>5</sub>
J <sub>1</sub>	40	30	50	50	58
J <sub>2</sub>	26	38	60	26	38
J <sub>3</sub>	40	34	28	24	30
J <sub>4</sub>	28	40	40	32	48
J <sub>5</sub>	28	32	38	22	44

Row minimization matrix is

10 0 20 20 28  
 0 12 34 0 12  
 16 10 4 0 6  
 0 12 12 4 20  
 6 10 16 0 22

Column minimization matrix is

10 0 16 20 22  
 0 12 30 0 6  
 16 10 0 0 0  
 0 12 8 4 14  
 6 10 12 0 16

In the above matrix all zeros can be covered with only four lines as follows

<del>10</del>	<del>0</del>	<del>16</del>	<del>20</del>	<del>22</del>
0	12	30	0	6
<del>16</del>	<del>10</del>	<del>0</del>	<del>0</del>	<del>0</del>
0	12	8	4	14
6	10	12	0	16

The least value in the uncrossed cells is 8. It is subtracted from the uncrossed cell and added for the intersection of the vertical line and horizontal lines

18 0 16 28 22  
 0 4 22 0 6  
 24 10 0 8 0  
 0 4 0 4 14  
 6 2 4 0 16

Since the above matrix can only be covers with '5' lines the assignment can be done as follows

	M <sub>1</sub>	M <sub>2</sub>	M <sub>3</sub>	M <sub>4</sub>	M <sub>5</sub>
J <sub>1</sub>	18	0	16	28	22
J <sub>2</sub>	0	4	22	0	6
J <sub>3</sub>	24	0	0	8	0
J <sub>4</sub>	0	4	0	4	14
J <sub>5</sub>	6	2	4	0	16

∴ Assignments of jobs are

J <sub>1</sub> - M <sub>2</sub>	J <sub>2</sub> - M <sub>1</sub>	J <sub>3</sub> - M <sub>5</sub>	J <sub>4</sub> - M <sub>3</sub>	J <sub>5</sub> - M <sub>4</sub>
30	38	28	28	22

∴ Total processing time = 30 + 38 + 28 + 28 + 22 = 146 minutes

50. In orthogonal turning of a cylindrical tube of wall thickness 5mm, the axial and the tangential cutting forces were measured at 1259 N and 1601 N, respectively. The measured chip thickness after machining was found to be 0.3 mm. The rake angel was 10° and the axial feed was 100 mm/min. The rotational speed of the spindle was 1000 rpm. Assuming the material to be perfectly plastic and Merchant's first solution, the shear strength of the martial is closest to
- (A) 722 MPa                      (B) 875 MPa                      (C) 200 MPa                      (D) 920 MPa

**Key: (A)**

**Sol:**  $F_t = 1259 \text{ N}$ ,  $F_c = 1601 \text{ N}$ ,  $t_c = 0.3 \text{ mm}$   
 $\alpha = 10^\circ$ ,  $F = 100 \text{ mm/min}$ ,  $N = 1000 \text{ rpm}$

$$f = \frac{F}{N} = \frac{100}{1000} = 0.1 \text{ mm / rev}$$

Since it is orthogonal machining

$$t = f = 0.1 \text{ mm}$$

$$r = \frac{t}{t_c} = \frac{0.1}{0.3} = 0.33$$

$$\tan \phi = \frac{r \cos \alpha}{1 - r \sin \alpha} = \frac{0.33 \cos 10}{1 - 0.33 \sin 10} = 0.348$$

$$\phi = 19.18^\circ$$

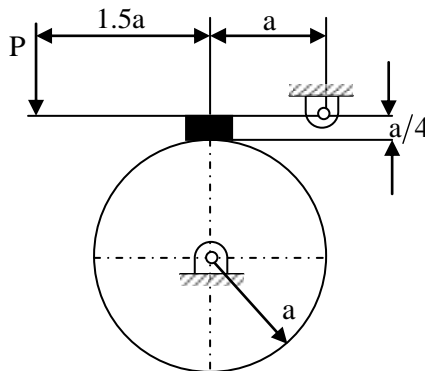
$$F_s = F_c \cos \phi - F_t \sin \phi$$

$$= 1601 \cos 19.18 - 1259 \sin 19.18 = 1098.42 \text{ N}$$

$$F_s = \tau bt / \sin \phi \Rightarrow 1098.42 = \frac{\tau \times 5 \times 0.1}{\sin(19.18)}$$

$$\therefore \tau = 721.74 \text{ MPa}$$

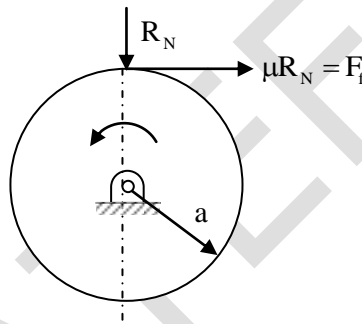
51. A single block brake with a short shoe and torque capacity of 250 N-m is shown. The cylindrical brake drum rotates anticlockwise at 100 rpm and the coefficient of friction is 0.25.



The value of  $a$ , in mm (round off to one decimal place), such that the maximum actuating force  $P$  is 2000 N, is \_\_\_\_\_.

**Key: (212.5)**

**Sol:** FBD of drum is



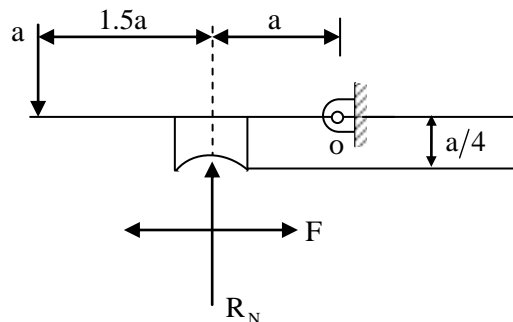
Given that Braking torque  $\tau_b = 250 \text{ N.m}$

$$\tau_b = F_f \times a$$

$$250 = F_f \times a \Rightarrow F_f = \frac{250}{a} \text{ N}$$

$$F_f = \mu R_N \Rightarrow R_N = \frac{F_f}{\mu} = \frac{250}{a(0.25)} = \frac{1000}{a} \text{ N}$$

FBD of lever is



$$\Sigma M_0 = 0 \Rightarrow P \times 2.5a = R_N \times a + F_f \times \frac{a}{4}$$

$$(2000) \times 2.5a = \frac{1000}{a} \times a + \frac{250}{a} \times \frac{a}{4}$$

$$5000a = 1000 + 62.5$$

$$a = 0.2125m = 212.5 \text{ mm}$$

52. A circular shaft having diameter  $65.00^{+0.01}_{-0.05}$  mm is manufactured by turning process. A  $50 \mu\text{m}$  thick coating of TiN is deposited on the shaft. Allowed variation in TiN film thickness is  $\pm 5\mu\text{m}$ . The minimum hole diameter (in mm) to just provide clearance fit is
- (A) 65.12                      (B) 64.95                      (C) 65.01                      (D) 65.10

**Key: (A)**

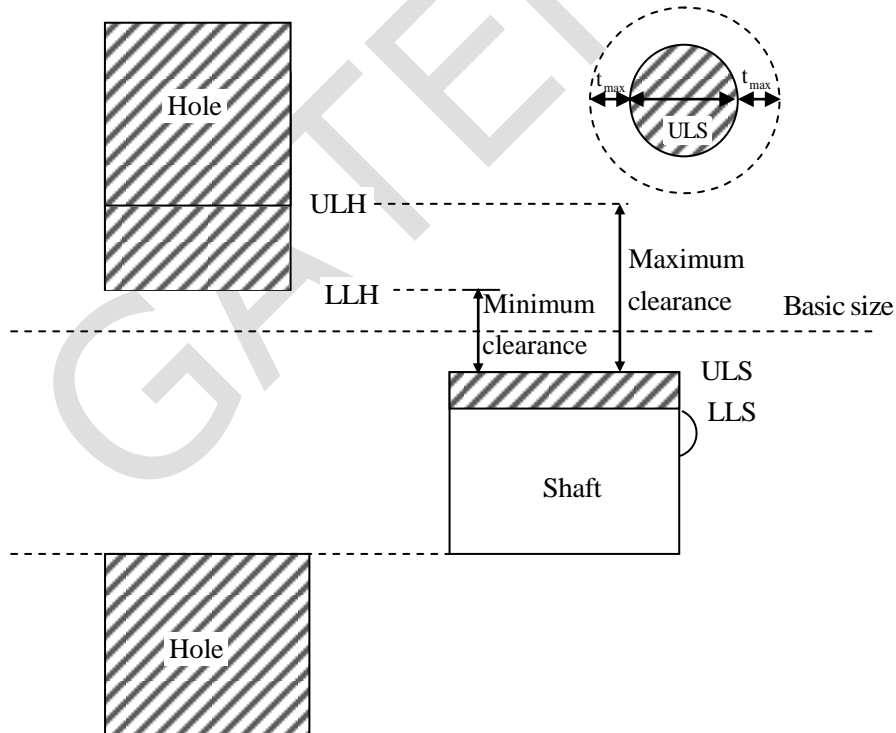
**Sol:** Shaft =  $65.12^{+0.01}_{-0.05}$

Coating thickness =  $50 \pm 5\mu\text{m}$

$55\mu\text{m} = 0.055\text{mm}$

or  $45\mu\text{m} = 0.045 \text{ mm}$

Clearance Fit



For just clearance Fit

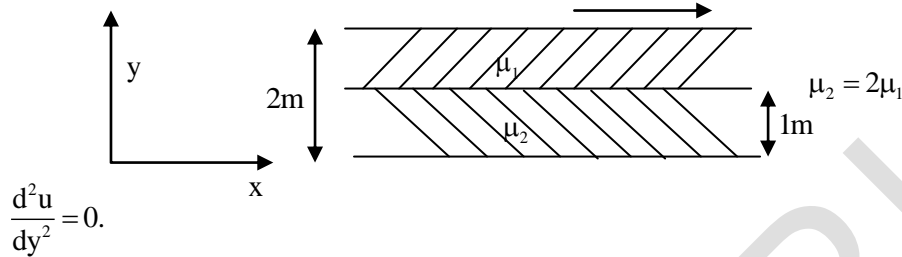
Minimum clearance = zero

$\therefore LLH = ULS$

$\therefore ULS \text{ before electro plating} = 65.01$

$\therefore ULS \text{ after electroplating} = 65.01 + 2 \times 0.055 = 65.12\text{mm}$

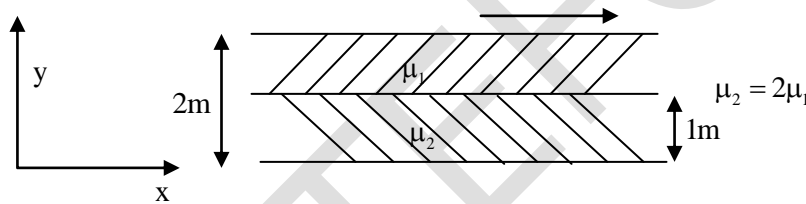
53. Two immiscible, incompressible, viscous fluids having same densities but different viscosities are contained between two infinite horizontal parallel plates, 2 m apart as shown below. The bottom plate is fixed and the upper plate moves to the right with a constant velocity of 3 m/s. With the assumptions of Newtonian fluid, steady, and fully developed laminar flow with zero pressure gradient in all directions, the momentum equations simplify to



If the dynamic viscosity of the lower fluid,  $\mu_2$ , is twice that of the upper fluid,  $\mu_1$ , then the velocity at the interface (round off to two decimal places) is \_\_\_\_\_ m/s.

**Key: (1)**

**Sol:**



Given that  $\frac{d^2u}{dy^2} = 0 \rightarrow (1)$

Integrating once, the above equation becomes

$$\frac{du}{dy} = C_1 \rightarrow (2)$$

Integrating equation (2),

$$u = C_1 y + C_2 \rightarrow (3)$$

From equation (3) we can say that, velocity is linearly varying so the shear stress will be constant at the interface of two viscous fluids

i.e., shear stress at  $y=1m$ , from fixed plate = shear stress at  $1m$  from moving plate.

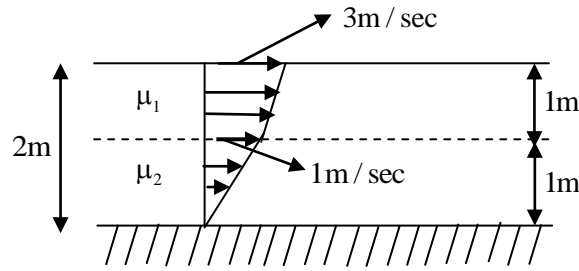
$$\mu_2 \left( \frac{v_2 - 0}{1} \right) = \mu_1 \left( \frac{v - v_i}{1} \right)$$

where  $v$  = velocity of moving plate,  $v_i$  = velocity at interface of two fluids

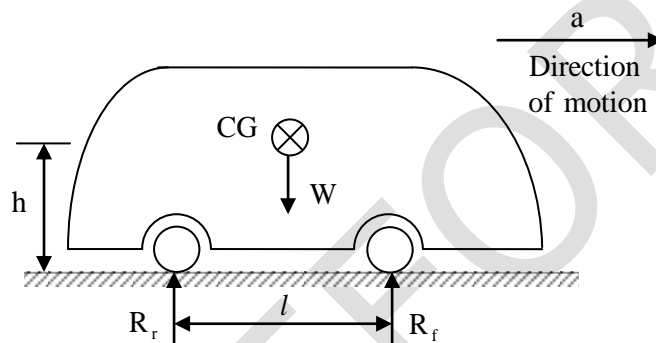
$$2\mu_1 \left( \frac{v_i}{1} \right) = \mu_1 \left( \frac{3 - v_i}{1} \right) \Rightarrow 2v_i = 3 - v_i \Rightarrow \boxed{v_i = 1m / sec}$$



Then the velocity profile will be as follows



54. A car having weight  $W$  is moving in the direction as shown in the figure. The centre of gravity (CG) of the car is located at height  $h$  from the ground, midway between the front and rear wheels.

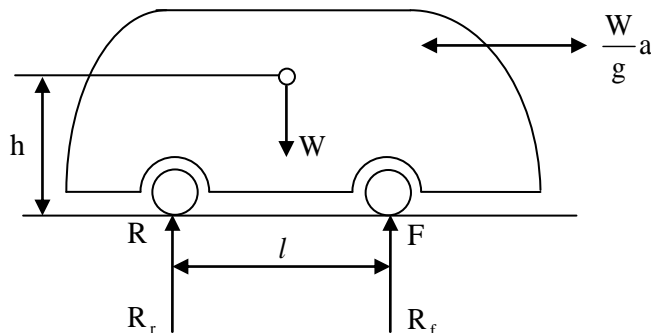


The distance between the front and rear wheels is  $l$ . The acceleration of the car is  $a$ , and acceleration due to gravity is  $g$ . The reactions on the front wheels ( $R_f$ ) and rear wheels ( $R_r$ ) are given by

- (A)  $R_f = R_r = \frac{W}{2} + \frac{W}{g} \left( \frac{h}{l} \right) a$   
 (B)  $R_f = \frac{W}{2} + \frac{W}{g} \left( \frac{h}{l} \right) a; R_r = \frac{W}{2} - \frac{W}{g} \left( \frac{h}{l} \right) a$   
 (C)  $R_f = R_r = \frac{W}{2} - \frac{W}{g} \left( \frac{h}{l} \right) a$   
 (D)  $R_f = \frac{W}{2} - \frac{W}{g} \left( \frac{h}{l} \right) a; R_r = \frac{W}{2} + \frac{W}{g} \left( \frac{h}{l} \right) a$

**Key: (D)**

**Sol:**



$$\Sigma M_y = 0$$

$$R_r + R_f = W \rightarrow (1)$$

$$\Sigma M_r = 0$$

$$\left( W \times \frac{L}{2} \right) - \left( \frac{W}{g} a \times h \right) - (R_f \times \ell) = 0$$

$$R_f = \frac{W}{2} - \frac{W}{g} \left( \frac{h}{L} \right) a$$

$$R_r = \frac{W}{2} + \frac{W}{g} \left( \frac{h}{L} \right) a.$$

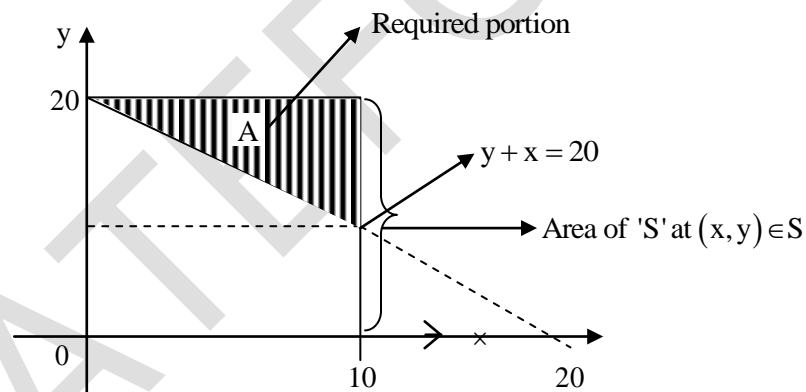
55. The variable  $x$  takes a value between 0 and 10 with uniform probability distribution. The variable  $y$  takes a value between 0 and 20 with uniform probability distribution. The probability of the sum of variables  $(x + y)$  being greater than 20 is

(A) 0.33                      (B) 0.50                      (C) 0.25                      (D) 0

**Key: (C)**

**Sol:**  $x \rightarrow [0, 10]$

$y \rightarrow [0, 20]$



$$P[x + y > 20] = ?$$

$$\therefore f(x, y) = \frac{1}{\text{Area of } S} = \frac{1}{200}$$

$$\therefore P[x + y > 20] = P[y > 20 - x]$$

$$= \frac{\text{area of } A}{\text{area of } S} = \frac{\frac{1}{2} \times 10 \times 10}{200} = \frac{1}{4} = 0.25$$

(or)

$$P[x + y > 20] = \iint_A f(x, y) dx dy = \iint_A \frac{1}{200} dx dy$$

$$= \frac{1}{200} \iint_A dx dy = \frac{1}{200} [\text{Area of triangle}]$$

$$= \frac{1}{200} \times \left[ \frac{1}{2} \times 10 \times 10 \right] = 0.25.$$