

**GENERAL APTITUDE**

**Q. No. 1 - 5 Carry One Mark Each**

1. Five different books (P, Q, R, S, T) are to be arranged on a shelf. The books R and S are to be arranged first and second, respectively from the right side of the shelf. The number of different order in which P, Q and T may be arranged is \_\_\_\_\_.

(A) 2                                      (B) 120                                      (C) 6                                      (D) 12

**Key: (D)**

**Sol:**                      (P, Q, T)                      S                      R  
                                   ↓                      ↓                      ↓  
                                   3 × 2 × 1  
                                   choices choices choice

∴ The number of different orders in which P, Q and T arranged =  $3 \times 2 \times 1 = 6$

2. The boat arrived \_\_\_\_\_ dawn.

(A) on                                      (B) at                                      (C) under                                      (D) in

**Key: (B)**

3. It would take one machine 4 hours to complete a production order and another machine 2 hours to complete the same order. If both machines work simultaneously at their respective constant rates, the time taken to complete the same order is \_\_\_\_\_ hours.

(A) 2/3                                      (B) 7/3                                      (C) 4/3                                      (D) 3/4

**Key: (C)**

**Sol:** Machine 1 takes to complete a work = 4 hours

$$\Rightarrow \text{Machine 1, 1 hour work} = \frac{1}{4}$$

Machine 2 takes to complete the same work = 2 hours

$$\Rightarrow \text{Machine 2, 1 hour work} = \frac{1}{2}$$

$$(\text{Machine 1} + \text{Machine 2}) \rightarrow 1 \text{ hour work} = \frac{1}{4} + \frac{1}{2} = \frac{3}{4}$$

$$\therefore \text{Required time} = \frac{\text{Total work}}{\text{1hr work}} = \frac{1}{\left(\frac{3}{4}\right)} = \frac{4}{3} \text{ hours}$$

4. When he did not come home, she \_\_\_\_\_ him lying dead on the roadside somewhere  
(A) concluded (B) pictured (C) notice (D) looked

**Key: (B)**

5. The strategies that the company \_\_\_\_\_ to sell its products \_\_\_\_\_ house-to-house marketing.  
(A) uses, include (B) use, includes (C) uses, including (D) used, includes

**Key: (A)**

**Q. No. 6 - 10 Carry Two Marks Each**

6. "Indian history was written by British historians – extremely well documented and researched, but not always impartial. History had to serve its purpose: Everything was made subservient to the glory of the Union Jack. Latter-day Indian scholar presented a contrary picture."

From the text above, we can infer that:

Indian history written by British historians \_\_\_\_\_.

- (A) was well documented and not researched but was always biased  
(B) was not well documented and researched and was sometimes biased  
(C) was well documented and researched but was sometimes biased  
(D) was not well documented and researched and was always biased

**Key: (C)**

7. Two design consultants, P and Q, started working from 8 AM for a client. The client budgeted a total of USD 3000 for the consultants. P stopped working when the hour hand moved by 210 degrees on the clock. Q stopped working when the hour hand moved by 240 degrees. P took two tea breaks of 15 minutes each during her shift, but took no lunch break. Q took only one lunch break for 20 minutes, but no tea breaks. The market rate for consultants is USD 200 per hour and breaks are not paid. After paying the consultants, the client shall have USD \_\_\_\_\_ remaining in the budget.

- (A) 000.00 (B) 433.33 (C) 166.67 (D) 300.00

**Key: (C)**

**Sol:** Given, P and Q started working from 8 A.M for a client

Total budget = USD 3000

P worked exactly 7 hours but took 30 min break.

'P' working number of hours = 6.5 hours

'Q' worked exactly 8 hours but took 20 min break.

'Q' working number of hours  $\approx$  7.67 hours

Client paying for both P and Q = USD 200/hr

$$\therefore \text{Total USD Paid} = 6.5 \times 200 + 7.67 \times 200 = 1300 + 1534 = 2834$$

After paying the consultants P and Q, the client shall have USD remaining in the budget  
= 3000 – 2834 ≈ 166

8. Five people P, Q, R, S and T work in a bank . P and Q don't like each other but have to share an office till T gets a promotion and moves to the big office next to the garden. R, who is currently sharing an office with T wants to move to the adjacent office with S, the handsome new intern. Given the floor plan, what is the current location of Q, R and T?

(O = Office, WR = Washroom)

(A)

WR	O1 P,Q	O2	O3 R,T	O4 S
Manager		Teller		Teller
		Entry		
Garden				

(B)

WR	O1 P,Q	O2	O3 R	O4 S
Manager T		Teller 1		Teller 2
		Entry		
Garden				

(C)

WR	O1 P	O2 Q	O3 R	O4 S
Manager		Teller 1		Teller 2
		Entry		
Garden				

(D)

WR	O1 P,Q	O2	O3 T	O4 R,S
Manager		Teller 1		Teller 2
		Entry		
Garden				

**Key: (A)**

**Sol:** According to the given data, Option (A) is correct.

9. Four people are standing in a line facing you. They are Rahul, Mathew, Seema and Lohit. One is an engineering, one is a doctor, one a teacher and another a dancer. You are told that:

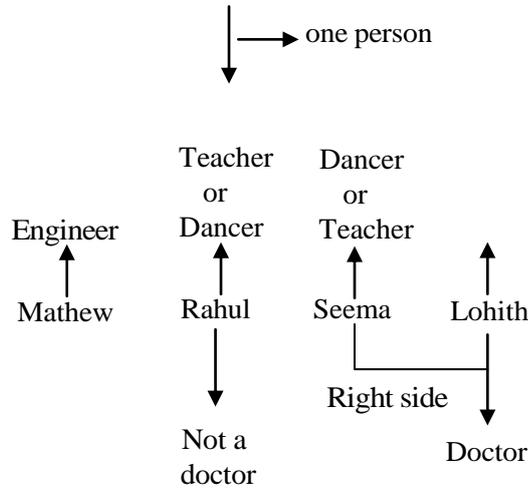
1. Mathew is not standing next to Seema
2. There are two people standing between Lohit and the engineer
3. Rahul is not a doctor
4. The teacher and the dancer are standing next to each other.
5. Seema is turning to her right to speak to the doctor standing next to her.

Who amongst them is an engineer?

- (A) Rahul                      (B) Mathew                      (C) Seema                      (D) Lohit

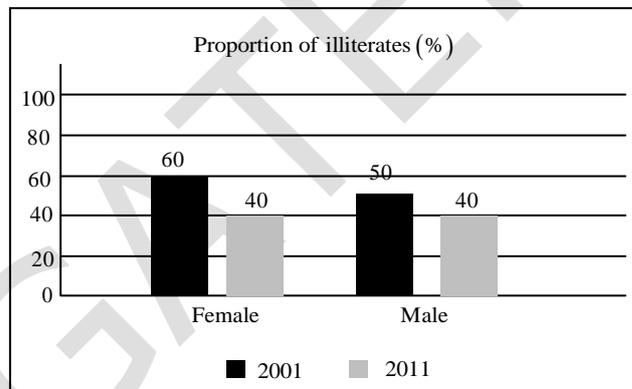
**Key: (B)**

**Sol:** According to the given data; we have

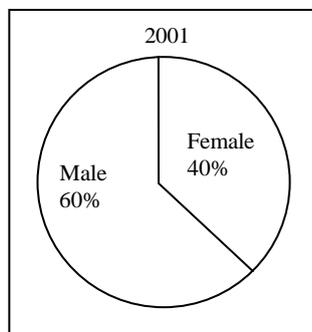


∴ **Mathew must be an Engineer.**

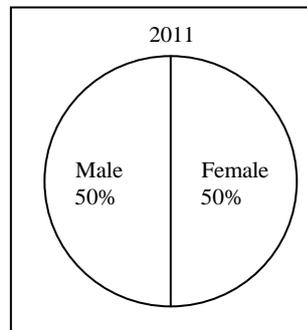
10. The bar graph in Panel (a) shows the proportion of male and female illiterates in 2001 and 2011. The proportions of males and females in 2001 and 2011 are given in Panel (b) and (c), respectively. The total population did not change during this period. The percentage increase in the total number of literate from 2001 to 2011 is \_\_\_\_\_.



Panel (a)



Panel (b)



Panel (c)

- (A) 33.43      (B) 35.43      (C) 34.43      (D) 30.43

**Key: (D)**

**Sol:** Let us assume, that population = 100 [2001–2011]

From panel (a);	From panel (b & c);
Percentage of male literates in 2001 = 50%	Number of males in 2001=60
Percentage of female literates in 2001 = 40%	Number of females in 2001=40
Percentage of male literates in 2011 = 60%	Number of males in 2011=50
Percentage of female literates in 2011 = 60%	Number of females in 2011=50

$$\therefore \text{Number of male literates in 2001} = 60 \times \frac{50}{100} = 30$$

$$\text{Number of female literates in 2001} = 40 \times \frac{40}{100} = 16$$

$$\text{Number of male literates in 2011} = 50 \times \frac{60}{100} = 30$$

$$\text{Number of female literates in 2011} = 50 \times \frac{60}{100} = 30$$

$$\text{Total number of literates in 2001} = 30 + 16 = 46$$

$$\text{Total number of literates in 2011} = 30 + 30 = 60$$

$\therefore$  Percentage increase in the total number of literates from 2001–2011

$$= \left[ \frac{60 - 46}{46} \times 100 \right] \% = \left[ \frac{14}{46} \times 100 \right] \% = 30.43\%$$



**ELECTRONICS & COMMUNICATION ENGINEERING**

**Q. No. 1 to 25 Carry One Mark Each**

1. Radiation resistance of a small dipole current element of length  $l$  at a frequency of 3 GHz is 3 ohms. If the length is changed by 1%, then the percentage change in the radiation resistance, rounded off two decimal places, is \_\_\_\_\_%.

**Key: (2)**

**Sol:** Given,  $R_{\text{rad}} = 3\Omega$ , and  $f = 3\text{GHz}$

$$\% \text{ change in length } \frac{d\ell}{\ell} \times 100\% = 1\%, \frac{dR_{\text{rad}}}{R_{\text{rad}}} \times 100\% = ?$$

$$R_{\text{rad}} = \frac{80\pi^2}{\lambda^2} \ell^2 \quad \dots(1)$$

$$\text{Change in resistance with respect to change in length is } = \frac{dR_{\text{rad}}}{d\ell} = 2\ell \left( \frac{80\pi^2}{\lambda^2} \right) \dots(2)$$

$$\frac{\text{Equation (2)}}{\text{Equation (1)}} = \frac{\frac{dR_{\text{rad}}}{d\ell}}{R_{\text{rad}}} = \frac{2\ell}{\ell^2} = \frac{2}{\ell}$$

$$\Rightarrow \frac{dR_{\text{rad}}}{R_{\text{rad}}} = 2 \times \frac{d\ell}{\ell}$$

$$\Rightarrow \frac{dR_{\text{rad}}}{R_{\text{rad}}} \times 100\% = 2 \times \left( \frac{\partial\ell}{\ell} \times 100\% \right) \rightarrow \% \text{ change in length} \quad \left[ \because \frac{d\ell}{\ell} \times 100\% = 1\% \right]$$

$\therefore$  % change in radiation resistance = 2%.

2. Which one of the following functions is analytic over the entire complex plane?

(A)  $\ln(z)$       (B)  $\cos(z)$       (C)  $e^{1/z}$       (D)  $\frac{1}{1-z}$

**Key: (B)**

**Sol:**  $\ln(z)$  is not analytic at  $z = 0$ ;

$e^{\frac{1}{z}}$  is not analytic at  $z = 0$  and

$\frac{1}{1-z}$  is not analytic at  $z = 0$ .

But  $\cos(z)$  is analytic over the entire complex plane,

$$\begin{aligned} \text{Since } \cos z &= \cos(x + iy) = \cos x \cos(iy) - (\sin x \sin(iy)) \\ &= \cos x \cosh y - i \sin x \sinh y; \rightarrow u + iv \text{ form} \end{aligned}$$

Where,  $u(x, y) = \cos x \cosh y$ ;  $v(x, y) = -\sin x \sinh y$

$$\begin{aligned} u_x = -\sin x \cdot \cosh y & \quad v_x = -\cos x \cdot \sinh y \\ u_y = \cos x \sinh y & \quad v_y = -\sin x \cdot \cosh y \end{aligned}$$

$\therefore u_x = v_y$  &  $u_y = -v_x \forall z$ .

3. The value of the integral  $\int_0^\pi \int_y^\pi \frac{\sin x}{x} dx dy$ , is equal to \_\_\_\_\_.

**Key: (2)**

**Sol:**  $\int_0^\pi \int_y^\pi \frac{\sin x}{x} dx dy$

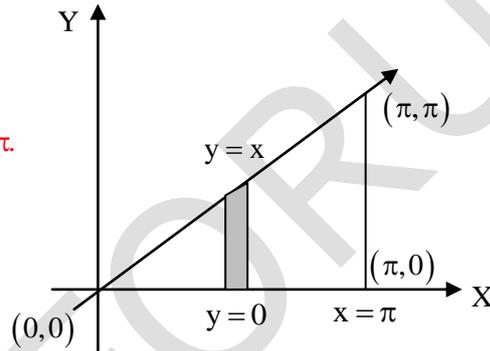
Given limits are  $x = y \rightarrow x = \pi$  &  $y = 0 \rightarrow y = \pi$ .

For change of order of integration,

Consider a strip parallel to Y-axis. Then

Limits of y are:  $y = 0 \rightarrow y = x$  and

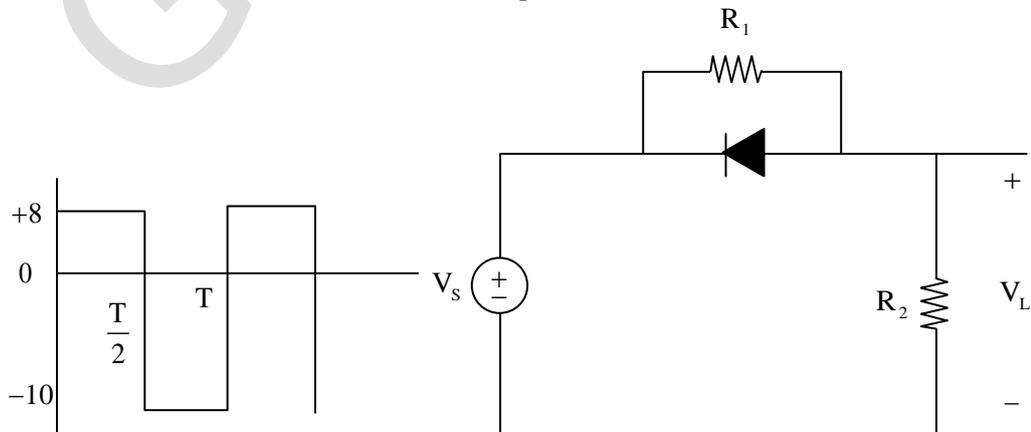
Limits of x:  $x = 0 \rightarrow x = \pi$



$$\begin{aligned} \therefore \int_0^\pi \int_y^\pi \frac{\sin x}{x} dx dy &= \int_{x=0}^\pi \left[ \int_{y=0}^x \frac{\sin x}{x} dy \right] dx = \int_{x=0}^\pi \frac{\sin x}{x} [y]_0^x dx = \int_{x=0}^\pi \sin x dx \\ &= [-\cos x]_0^\pi = -[\cos \pi - \cos 0] = -[-1 - 1] = 2 \end{aligned}$$

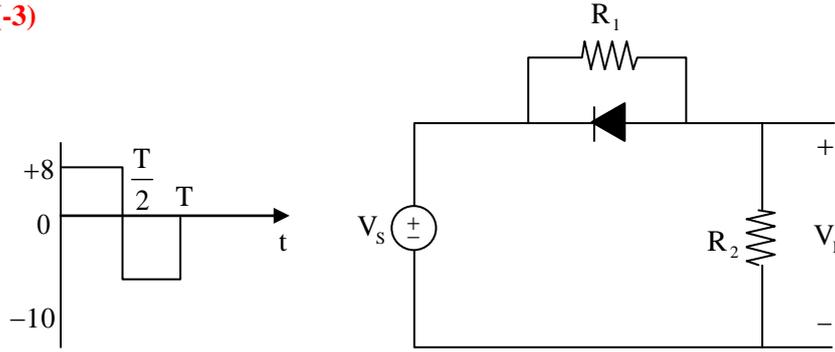
$$\Rightarrow \int_0^\pi \int_y^\pi \frac{\sin y}{x} dx dy = 2$$

4. In the circuit shown,  $V_s$  is a square wave of period  $T$  with maximum and minimum values of  $8V$  and  $-10V$ , respectively, Assume that the diode is ideal and  $R_1 = R_2 = 50\Omega$ . The average value of  $V_L$  is \_\_\_\_\_ volts (rounded off to 1 decimal place).

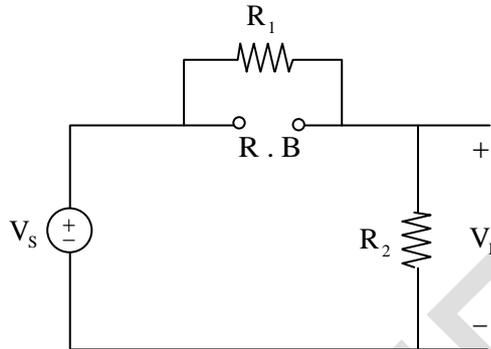


**Key: (-3)**

**Sol:**



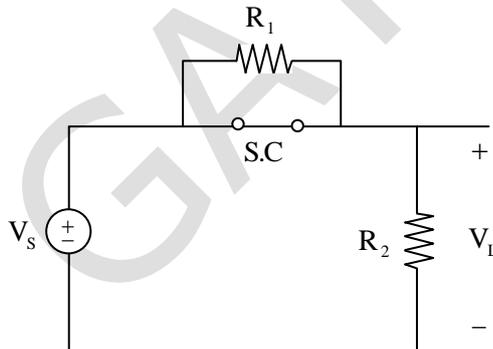
Case (i) For +ve half cycle diode is reverse bias:



$$V_L = \frac{R_2}{R_1 + R_2} \cdot V_s = \frac{50}{100} \times 8V = 4V$$

Case (ii):

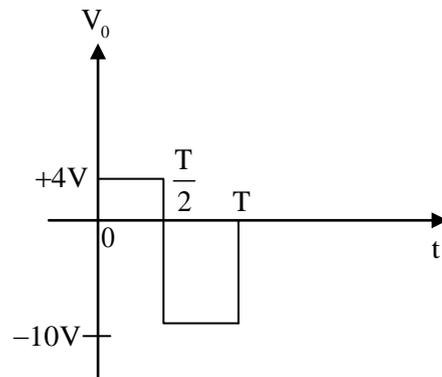
For negative half cycle diode is forward bias and ideally act as short circuit.



$V_L = V_s = -10V$ . So, output waveform is

$$V_{avg} = \frac{4V \times \frac{T}{2} + (-10V \times \frac{T}{2})}{T} = 2V - 5V = -3V$$

$\therefore V_{avg} = -3V$





$\Rightarrow ydy = -x dx \rightarrow$  variable-separable D.E

Integrating on both sides; we get

$$\frac{y^2}{2} = -\frac{x^2}{2} + c \Rightarrow \frac{x^2}{2} + \frac{y^2}{2} = c$$

$$\Rightarrow x^2 + y^2 = c$$

$$\Rightarrow x^2 + y^2 = (\sqrt{c})^2; \text{ which represents family of circles}$$

7. In the table shown, List-I and List-II, respectively, contain terms appearing on the left-hand side and the right-hand side of Maxwell's equations (in their standard form). Match the left-hand side with the corresponding right-hand side.

List-I		List-II	
1.	$\nabla \cdot D$	(P)	0
2.	$\nabla \times E$	(Q)	$\rho$
3.	$\nabla \cdot B$	(R)	$-\frac{\partial B}{\partial t}$
4.	$\nabla \times H$	(S)	$J + \frac{\partial D}{\partial t}$

(A) 1-Q, 2-R, 3-P, 4-S

(B) 1-Q, 2-S, 3-P, 4-R

(C) 1-P, 2-R, 3-Q, 4-S

(D) 1-R, 2-Q, 3-S, 4-P

**Key: (A)**

**Sol:**  $\nabla \cdot D = \rho$

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{H} = \vec{J} + \frac{\partial \vec{D}}{\partial t}$$

$\therefore$  1-Q, 2-R, 3-P, 4-S  $\rightarrow$  Option (A) is correct

8. Consider the signal  $f(t) = 1 + 2\cos(\pi t) + 3\sin\left(\frac{2\pi}{3}t\right) + 4\cos\left(\frac{\pi}{2}t + \frac{\pi}{4}\right)$ , where  $t$  is in seconds. Its fundamental time period, in seconds, is \_\_\_\_\_.

**Key: (12)**

**Sol:** It is given that,

$$f(t) = 1 + 2\cos \pi t + 3\sin \frac{2\pi}{3}t + 4\cos \left(\frac{\pi}{2}t + \frac{\pi}{4}\right)$$

Its fundamental frequency  $\omega_0$

$$\omega_0 = \frac{\text{HCF}(\pi, 2\pi, \pi)}{\text{LCM}(1, 3, 2)} = \frac{\pi}{6}$$

$$T_0 = \frac{2\pi}{\omega_0} = \frac{2\pi \times 6}{\pi} = 12 \text{ sec}$$

9. If X and Y are random variables such that  $E[2X + Y] = 0$  and  $E[X + 2Y] = 33$ , the  $E[X] + E[Y] =$  \_\_\_\_\_.

**Key: (11)**

**Sol:** Given,  $E[2x + y] = 0$  &  $E[x + 2y] = 33$

$$\Rightarrow 2E(x) + E(y) = 0 \dots (1)$$

$$\Rightarrow E(x) + 2E(y) = 33 \dots (2)$$

Solving (1) and (2); we have

$$2E(x) + E(y) = 0$$

$$2E(x) + 4E(y) = 66 \quad [\because \text{equation (2) multiplied by 2}]$$

$$\hline -3E(y) = -66 \Rightarrow E(y) = 22$$

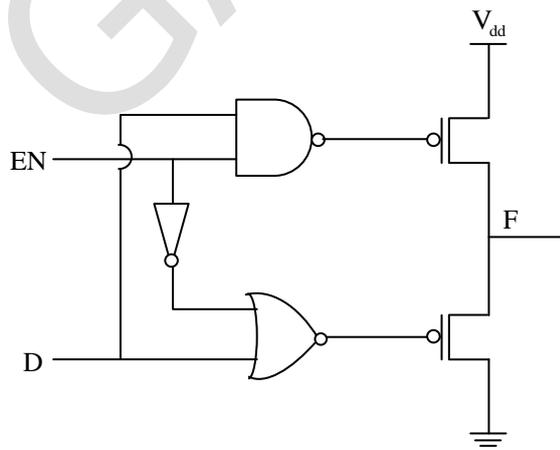
From (1);

$$2E(x) + E(y) = 0 \Rightarrow 2E(x) = -E(y)$$

$$\Rightarrow 2E(x) = -22 \Rightarrow E(x) = -11$$

$$\therefore E[x] + E[y] = -11 + 22 = 11 \Rightarrow E(x) + E(y) = 11$$

10. In the circuit shown, what are the values of F for EN = 0 and EN = 1, respectively?

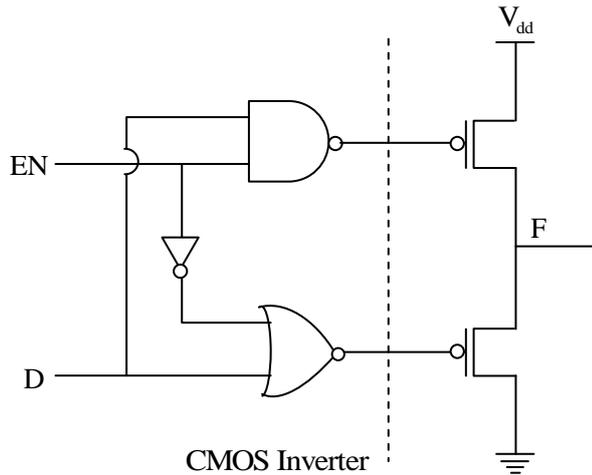


- (A) 0 and 1  
(C) 0 and D

- (B) Hi - Z and  $\bar{D}$   
(D) Hi - Z and D

**Key: (D)**

**Sol:**



→ NAND gate enabled, when their enable input is “1” and NOR gate enabled, when their enable input is “0”.

Case (i):

When  $EN = 0$ , the both the logic gates NAND and NOR disabled, so CMOS inverter input is floating. So, output is also high impedance state.

$$F = Hi - z$$

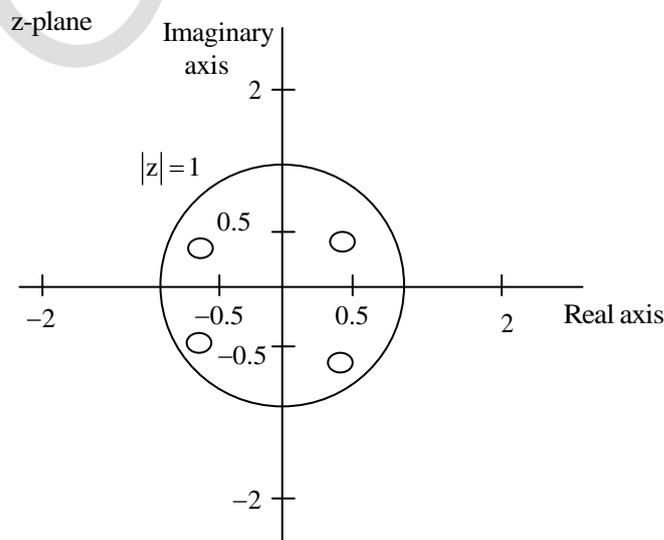
Case (ii):

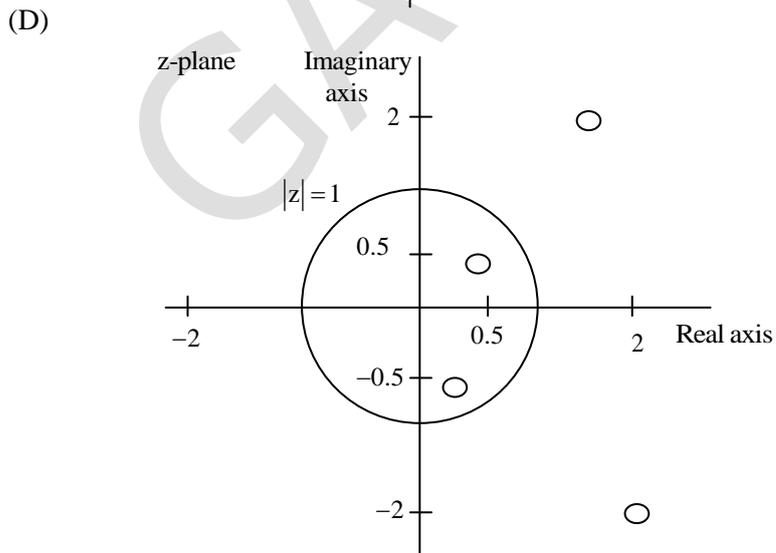
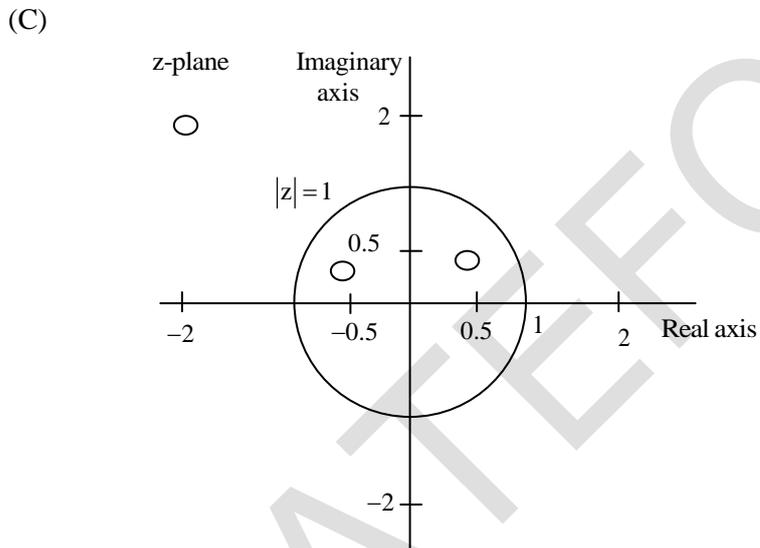
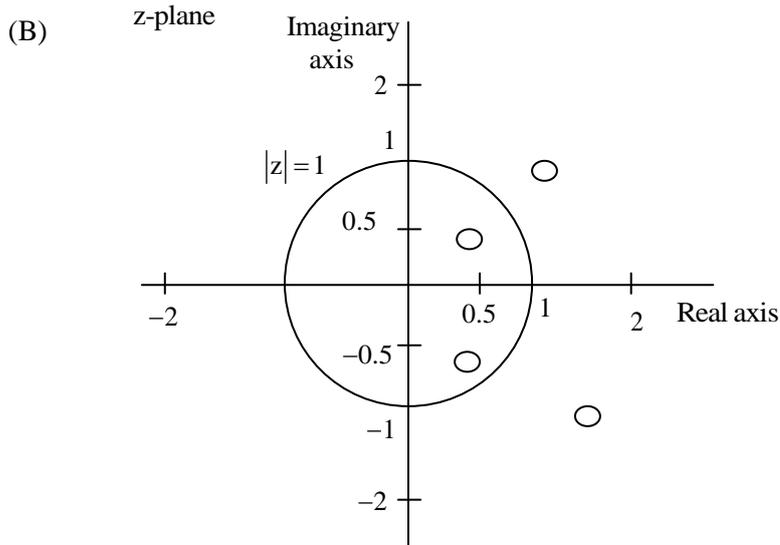
When  $EN = 1$ , then both the logic gates NAND and NOR are enabled with output  $\bar{D}$  that is input of CMOS inverter.

$$\text{So, } F = \bar{\bar{D}} = D$$

11. Let  $H(z)$  be the z-transform of a real-valued discrete time signal  $h[n]$ . If  $P(z) = H(z)H\left(\frac{1}{z}\right)$  has a zero  $z = \frac{1}{2} + \frac{1}{2}j$ , and  $P(z)$  has a total of four zeros, which one of the following plots represents all the zeros correctly?

(A)





**Key: (B)**

**Sol:** It is given that  $H(z)$  is z-transform of a real-valued signal  $h(n)$ .

$P(z) = H(z)H\left(\frac{1}{z}\right)$  and  $P(z)$  has 4 zeros we can say zeros of  $P(z)$  are, sum of zeros of  $H(z)$  and zeros of  $H\left(\frac{1}{z}\right)$

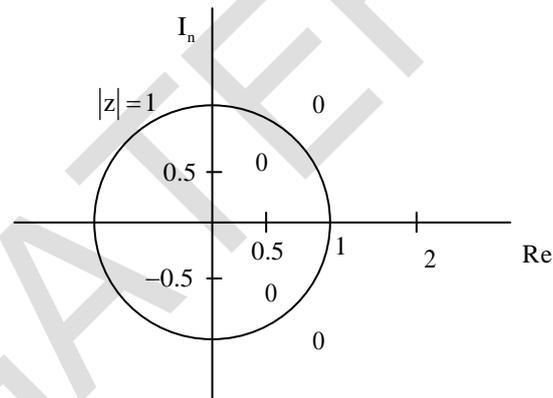
If  $z_1 = \frac{1}{2} + j\frac{1}{2}$  is one zero then there must be a zero at  $z_1^* = \frac{1}{2} - j\frac{1}{2}$

Let  $z_1, z_1^*$  represent zeros of  $H(z)$  then the zeros of  $H\left(\frac{1}{z}\right)$  will be  $\frac{1}{z_1}$  and  $\left(\frac{1}{z_1}\right)^*$

$$\frac{1}{z_1} = \frac{1}{\frac{1}{2} + j\frac{1}{2}} = 1 - i$$

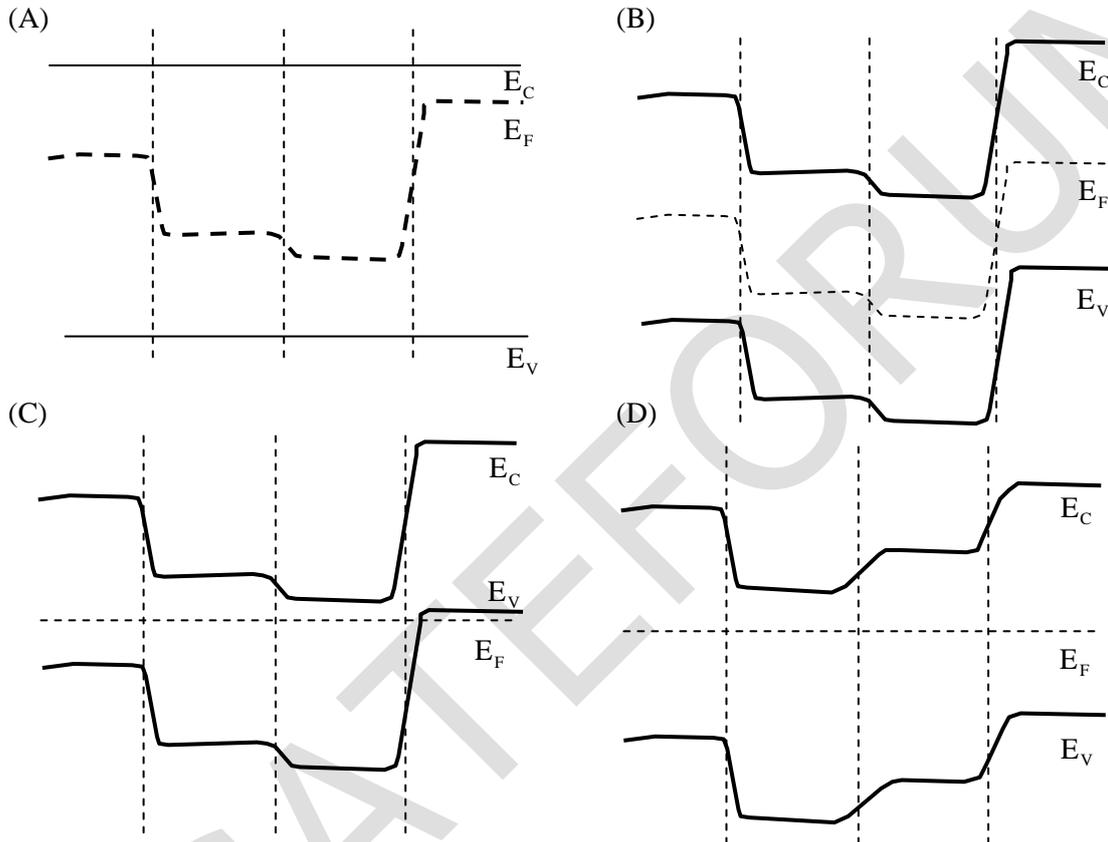
$$\left(\frac{1}{z_1}\right)^* = 1 + j$$

So the 4 zeros of  $P(z)$  are  $\left(\frac{1}{2} \pm j\frac{1}{2}\right)$  and  $(1 \pm j)$  or  $[0.707|\pm 45^\circ]$  and  $[\sqrt{2}|\pm 45^\circ]$



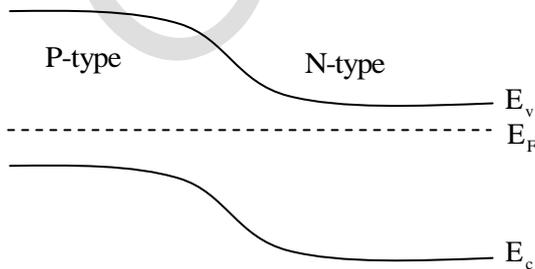
Even option D looks like similar but in option B, the zeros that are outside the unit circle have real part 2, but we need 1.

12. Which one of the following options describes correctly the equilibrium band diagram at  $T= 300$  K of a Silicon  $pnn^+p^{++}$  configuration shown in the figure?



**Key: (C)**

**Sol:** Typical energy band diagram of P-N junction diode:



- First of all of equilibrium, Fermi energy level ( $E_F$ ) is constant
- For P-type of semiconductor

$$E_F = E_v - kT \ln \left( \frac{N_A}{N_v} \right) \quad (\text{For } N_A < N_v)$$

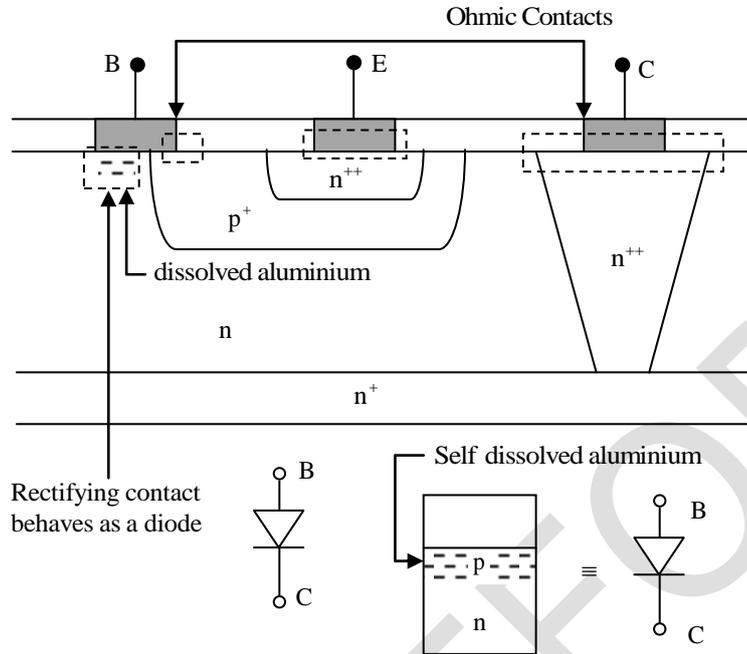
- For  $pnn^+p^{++}$  configuration, Fermi-energy level ( $E_F$ ) is more closer to  $E_v$  compare to  $E_c$ .



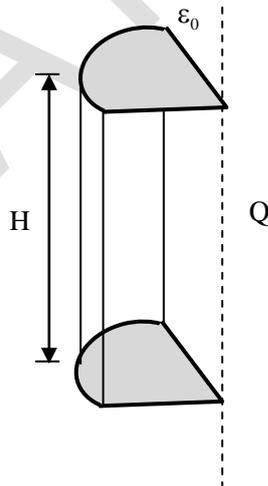


**Key: (D)**

**Sol:** Aluminum metal in contact with a lightly doped n type silicon forms a non ohmic rectifying contact because the trivalent aluminium easily dissolves into silicon and convert the part of n type semiconductor into p type.



15. What is the electric flux ( $\int \vec{E} \cdot d\vec{a}$ ) through a quarter-cylinder of height  $H$  (as shown in the figure) due to an infinitely long the line charge along the axis of the cylinder with a charge density of  $Q$ ?



- (A)  $\frac{4H}{Q\epsilon_0}$       (B)  $\frac{HQ}{4\epsilon_0}$       (C)  $\frac{HQ}{\epsilon_0}$       (D)  $\frac{H\epsilon_0}{4Q}$

**Key: (B)**

**Sol:** The total electric flux leaving the total cylinder of height “H” is

$$= \oiint \vec{E} \cdot d\vec{A} = \frac{QH}{\epsilon_0}$$

∴ The electric through a quarter cylinder of height “H” is

$$= \frac{\oiint \vec{E} \cdot d\vec{A}}{4} = \frac{QH}{4\epsilon_0}$$

∴ Option (B) is correct.

16. Let Z be an exponential random variable with mean 1. That is, the cumulative distribution function of Z is given by

$$F_z(x) = \begin{cases} 1 - e^{-x} & \text{if } x \geq 0 \\ 0 & \text{if } x < 0 \end{cases}$$

The  $\Pr(Z > 2 | Z > 1)$ , rounded off to two decimal places, is equal to \_\_\_\_\_.

**Key: (0.37)**

**Sol:** Given,

$$\text{Cumulative distribution function, } F_z(x) = \begin{cases} 1 - e^{-x} & \text{if } x \geq 0 \\ 0 & \text{if } x < 0 \end{cases}$$

$$\Rightarrow F'_z(x) = f_z(x) = \begin{cases} e^{-x}; & x \geq 0 \\ 0; & x < 0 \end{cases} \rightarrow \text{probability density function}$$

Where Z be an exponential R.V with mean ‘1’

$$\therefore \Pr\left[\frac{z > 2}{z > 1}\right] = \frac{\Pr[z > 2 \cap z > 1]}{\Pr[z > 1]} \quad [\text{Using conditional probability}]$$

$$= \frac{\Pr[z > 2]}{\Pr[z > 1]} = \frac{\int_2^{\infty} f(x) dx}{\int_1^{\infty} f(x) dx} = \frac{\int_2^{\infty} e^{-x} dx}{\int_1^{\infty} e^{-x} dx}$$

$$\Rightarrow \Pr\left[\frac{z > 2}{z > 1}\right] = \frac{[-e^{-x}]_2^{\infty}}{[-e^{-x}]_1^{\infty}} = \frac{[0 + e^{-2}]}{[0 + e^{-1}]} = \frac{e^{-2}}{e^{-1}} = \frac{1}{e} \approx 0.37$$

17. A linear Hamming code is used to map 4-bit messages to 7-bit codewords. The encoder mapping is linear. If the message 0001 is mapped to the codeword 0000111, and the message 0011 is mapped to the codeword 1100110, then the message 0010 is mapped to

- (A) 0010011                      (B) 1111111                      (C) 1111000                      (D) 1100001

**Key: (D)**

**Sol:** Message (1)  $\Rightarrow$  0001

Message (2)  $\Rightarrow$  0011

0000111  $\Rightarrow$  Codeword (1)

1100110  $\Rightarrow$  Codeword (2)

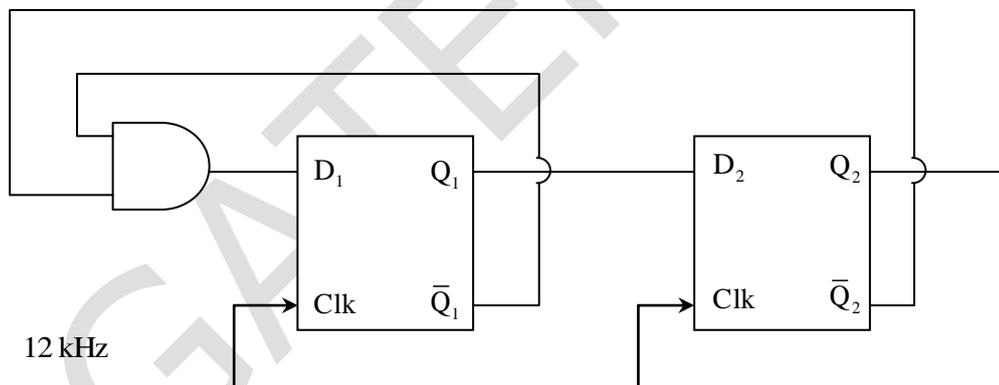
Since it is a linear hamming code,

Message (1) + Message (2) results in codeword (1) + codeword (2)

$\Rightarrow$  Addition of binary is logical XOR

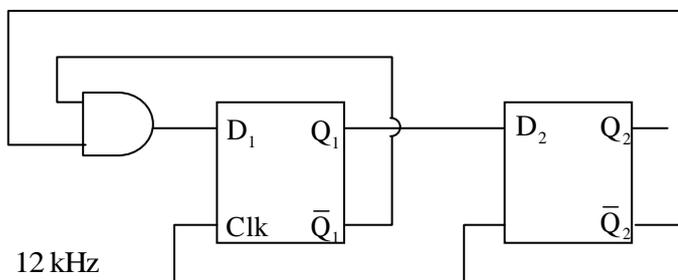
$\therefore$	Message		Codeword
	0 0 0 1		0 0 0 0 1 1 1
	⊕ 0 0 1 1		⊕ 1 1 0 0 1 1 0
	0 0 1 0		1 1 0 0 0 0 1
	↑		↑
	Message (3)		Codeword (3)

18. In the circuit shown, the clock frequency, i.e., the frequency of the Clk signal, is 12 kHz. The frequency of the signal at  $Q_2$  is \_\_\_\_\_ kHz.



**Key: (4)**

**Sol:**



$D_2(Q_1)$	$D_1(\bar{Q}_1, \bar{Q}_2)$	$Q_2$	$Q_1$
—	—	0	0
0	1	0	1
1	0	1	0
0	0	0	0

← Initially  
 1<sup>st</sup> clock  
 2<sup>nd</sup> clock  
 3<sup>rd</sup> clock

$$Q_2 Q_1 \rightarrow 00 \rightarrow 01 \rightarrow 10 \rightarrow 00$$

It is a MOD-3 synchronous counter

$$\text{So, } f_{Q_2} = \frac{f_i}{3} = \frac{12\text{kHz}}{3} = 4\text{ kHz}$$

19. A standard CMOS inverter is designed with equal rise and fall times ( $\beta_n = \beta_p$ ). If the width of the pMOS transistor in the inverter is increased, what would be the effect on the LOW noise margin ( $NM_L$ ) and the HIGH noise margin  $NM_H$ ?
- (A)  $NM_L$  increases and  $NM_H$  decrease      (B) Both  $NM_L$  and  $NM_H$  increase  
 (C) No change in the noise margins      (D)  $NM_L$  decreases and  $NM_H$  increases

**Key: (A)**

**Sol:** Given,  $\beta_n = \beta_p$  for standard CMOS inverter

We know that, standard definition of noise margin

$$NM_L = V_{IL} - V_{OLU}$$

$$NM_H = V_{OHU} - V_{IH}$$

**Case(i):**

$$\beta_n = \beta_p, \text{ let take } V_{DD} = 5, V_{TN} = -V_{TP} = 0.8, V_I = 2.5$$

$$V_{IL} = V_{TN} + \frac{3}{8}[V_{DD} + V_{TP} - V_{TN}] = 2.075$$

$$V_{OLU} = \frac{1}{2}[2V_{IH} - V_{DD} - V_{TN} - V_{TP}] = 0.45$$

$$(N_M)_L = V_{IL} - V_{OLU} = 1.625$$

$$V_{OHU} = \frac{1}{2}[2V_{IL} + V_{DD} - V_{TN} - V_{TP}] = 4.575$$

$$V_{IH} = V_{TN} + \frac{5}{8}[V_{DD} + V_{TP} - V_{TN}] = 2.95$$

$$(N_M)_H = 1.625$$

**Case (ii):** ( $\beta_n \neq \beta_p$ ) Because width of PMOS increased

$$\left(\frac{W}{L}\right)_p > \left(\frac{W}{L}\right)_n$$

$$\frac{\beta_p}{P_n} > 1, \frac{\beta_n}{\beta_p} < 1, \text{ Let assume } 0.8$$

$$V_{IL} = V_{TN} + \frac{V_{DD} + V_{TP} - V_{TN}}{\left(\frac{\beta_n}{\beta_p} - 1\right)} \left[ 2 \sqrt{\frac{\frac{\beta_n}{\beta_p}}{\frac{\beta_n}{\beta_p} - 3}} - 1 \right] = 2.216$$

$$V_{OLU} = \frac{V_{IH} \left(1 + \frac{\beta_n}{\beta_p}\right) - V_{DD} - \left(\frac{\beta_n}{\beta_p}\right)(V_{TN} - V_{TP})}{2 \left(\frac{\beta_n}{\beta_p}\right)}$$

$$= \frac{3.048 \times 1.8 - 5 - 0.64 + 0.8}{2 \times 0.8}$$

$$= 0.404$$

$$(NM)_L = 2.216 - 0.404 = 1.812 \text{ (Increased)}$$

$$V_{OUH} = \frac{1}{2} \left[ 1 + \left(\frac{\beta_n}{\beta_p}\right) V_{IL} + V_{DD} - \left(\frac{\beta_n}{\beta_p}\right) V_{TN} - V_{TP} \right]$$

$$= \frac{1}{2} [(2.216)1.8 + 5 - 0.64 + 0.8] = 4.574$$

$$V_{IH} = V_{TN} + \frac{(V_{DD} + V_{TP} - V_{TN})}{\frac{\beta_n}{\beta_p} - 1} \left[ \frac{2 \frac{\beta_n}{\beta_p}}{\sqrt{3 \frac{\beta_n}{\beta_p} + 1}} - 1 \right]$$

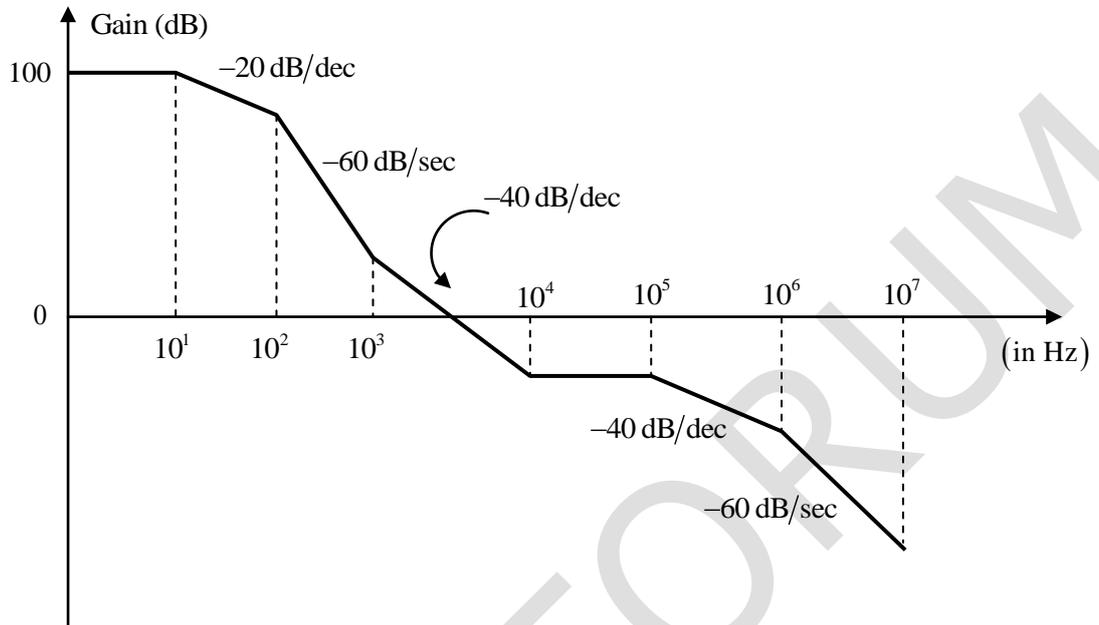
$$= 0.8 + \frac{[5 - 1.6]}{-0.2} \times -0.132$$

$$= 2.248 + 0.8 = 3.048$$

$$(NM)_H = 4.574 - 3.048$$

$$= 1.526 \text{ (decreased)}$$

20. For an LTI system, the Bode plot for its gain is as illustrated in the figure shown. The number of system poles  $N_p$  and the number of system zeros  $N_z$  in the frequency range  $1\text{ Hz} \leq f \leq 10^7\text{ Hz}$  is



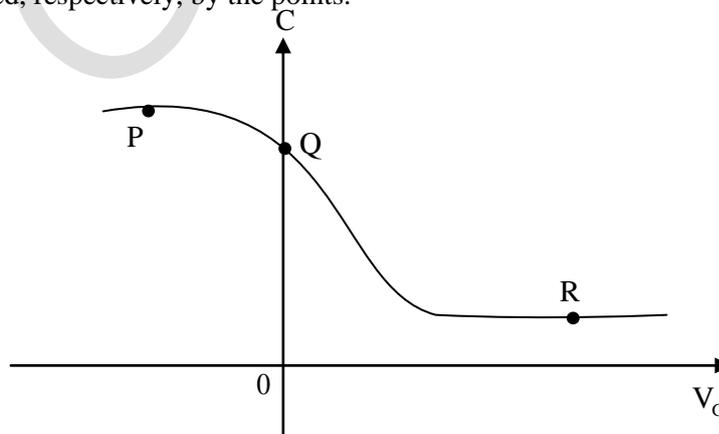
- (A)  $N_p = 4, N_z = 2$                       (B)  $N_p = 7, N_z = 4$   
(C)  $N_p = 6, N_z = 3$                       (D)  $N_p = 5, N_z = 2$

**Key: (C)**

**Sol: From the given plot**

$$N_p = 6, N_z = 3$$

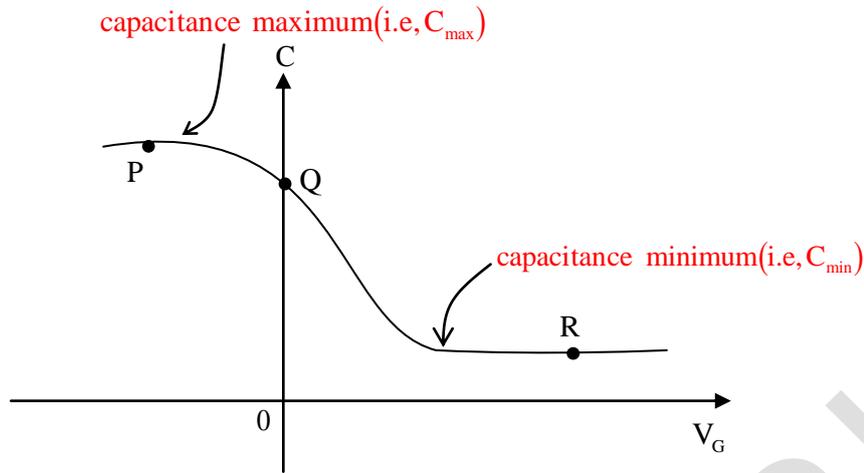
21. The figure shows the high-frequency C-V curve of a MOS capacitor (at  $T=300\text{ K}$ ) with  $\Phi_{ms} = 0\text{ V}$  and no oxide charges. The flat-band, inversion, and accumulation conditions are represented, respectively, by the points.



- (A) R,P,Q                      (B) Q,P,R                      (C) P,Q,R                      (D) Q,R,P

**Key: (D)**

**Sol:**



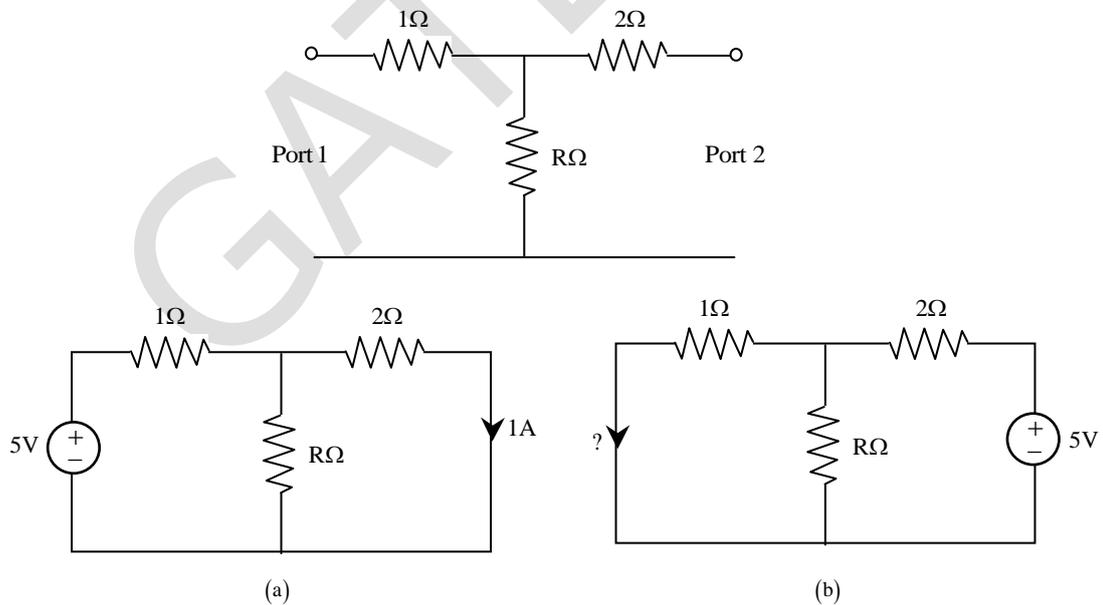
At higher frequency  $C_{min}$  minimum capacitance obtained in inversion-regime so point R belongs to inversion regime.

Maximum capacitance obtained in accumulation regime so point p-line is accumulation regime.

For  $\phi_m = 0V$ , flat band occurs at  $V_G = 0V$ , so point  $\phi$  lies at flat-band regime.

22. Consider the two-port resistive network shown in the figure. When an excitation of 5V is applied across Port 1, and Port 2 is shorted, the current through the short circuit at Port 2 is measured to be 1 A (see (a) in the figure).

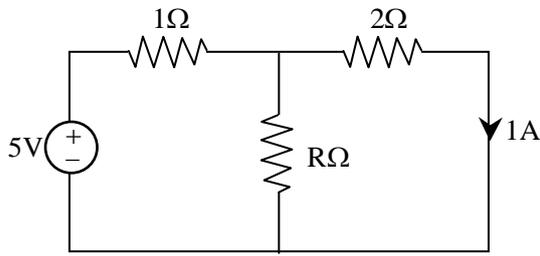
Now, if an excitation of 5 V is applied across port 2, and port 1 is shorted (see (b) in the figure), what is the current through the short circuit at port 1?



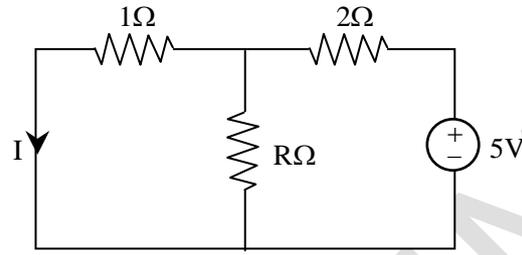
- (A) 1A                      (B) 2A                      (C) 2.5A                      (D) 0.5A

**Key: (A)**

**Sol:**



(figure a)



(figure b)

By reciprocity theorem, by referring (figure a),

We can say current I in (figure b) will be 1A.

$$\left[ \frac{V}{I} = k, \frac{V_1}{V_2} = \frac{I_1}{I_2} \right]$$

23. Let  $Y(s)$  be the unit-step response of a causal system having a transfer function

$$G(s) = \frac{3-s}{(s+1)(s+3)}$$

That is,  $Y(s) = \frac{G(s)}{s}$ . The forced response of the system is

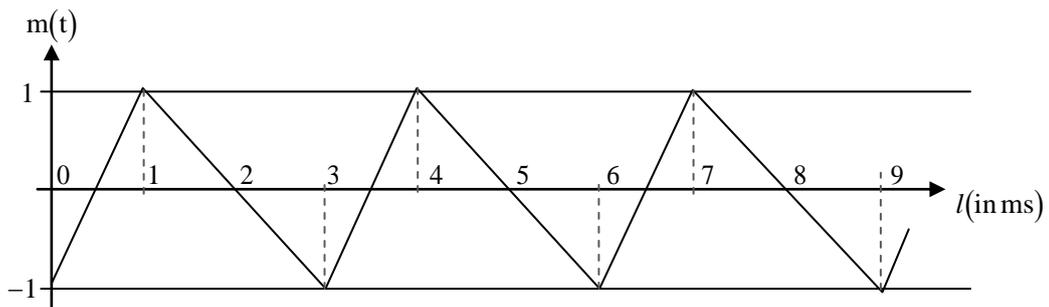
- (A)  $u(t) - 2e^{-t}u(t) + e^{-3t}u(t)$       (B)  $2u(t)$   
 (C)  $u(t)$       (D)  $2u(t) - 2e^{-t}u(t) + e^{-3t}u(t)$

**Key: (A)**

**Sol:** Forced response is the response, due to external input signal

$$\begin{aligned} Y(s) &= \frac{G(s)}{s} = \frac{3-s}{s(s+1)(s+3)} \\ &= \frac{1}{s} + \frac{-2}{s+1} + \frac{1}{s+3} \\ \Rightarrow y(t) &= u(t) - 2e^{-t}u(t) + e^{-3t}u(t) \end{aligned}$$

24. The baseband signal  $m(t)$  shown in the figure is phase-modulated to generate the PM signal  $\varphi(t) = \cos(2\pi f_c t + km(t))$ .



The time  $t$  on the  $x$ -axis in the figure is in milliseconds. If the carrier frequency is  $f_c = 50$  kHz and  $k = 10\pi$ , the ratio of the minimum instantaneous frequency (in kHz) to the maximum instantaneous frequency (in kHz) is \_\_\_\_\_ (rounded off to 2 decimal places).

**Key: (0.75)**

**Sol:** Instantaneous frequency  $(f_i) = \frac{1}{2\pi} \frac{d\theta(t)}{dt}$

$$\theta(t) = 2\pi f_c t + km(t)$$

$$\therefore f_i = \frac{1}{2\pi} \frac{d}{dt} [2\pi f_c t + km(t)] = f_c + \frac{K}{2\pi} \frac{dm}{dt}$$

$$f_{i_{\max}} = f_c + \frac{K}{2\pi} \frac{dm}{dt} \Big|_{\max} ; \quad f_{i_{\min}} = f_c + \frac{K}{2\pi} \frac{dm}{dt} \Big|_{\min}$$

$$\frac{dm}{dt} \Big|_{\max} = 2 \frac{dm}{dt} \Big|_{\min} = -1$$

$$f_{i_{\max}} = 50K + (5)(2)K = 60K$$

$$f_{i_{\min}} = (50K) + (5)(-1)K = 45K$$

$$\frac{f_{i_{\min}}}{f_{i_{\max}}} = \frac{45K}{60K} = \frac{3}{4} = 0.75$$

25. The value of the contour integral

$$\frac{1}{2\pi j} \oint \left( z + \frac{1}{z} \right)^2 dz$$

Evaluated over the unit circle  $|z|=1$  is \_\_\_\_\_.

**Key: (0)**

**Sol:**  $\frac{1}{2\pi j} \oint \left( z + \frac{1}{z} \right)^2 dz = \frac{1}{2\pi j} \oint \frac{(z^2 + 1)^2}{z^2} dz \quad \dots(1)$

$\therefore$  Singular point  $z=0$ ; which lies inside unit circle  $|z|=1$

$\therefore$  Using Cauchy's generalization integration formula, we have

$$\oint_c \frac{f(z)}{(z-z_0)^n} dz = 2\pi j \frac{[f^{(n-1)}(z_0)]}{(n-1)!}$$

$$\Rightarrow \therefore \oint_c \frac{(z^2 + 1)^2}{(z-0)^2} dz = 2\pi j \frac{[(z^2 + 1)^2]'}{1!} \Big|_{z=0}; \quad ' \rightarrow \text{denotes first derivative}$$

$$= 2\pi j [2(z^2 + 1)(2z)] \Big|_{z=0} = 2\pi j [0] = 0.$$

From(1),

$$\frac{1}{2\pi j} \oint \left( z + \frac{1}{z} \right)^2 dz = \frac{1}{2\pi j} \oint \frac{(z^2 + 1)^2}{(z-0)^2} dz = \frac{1}{2\pi j} (0) = 0$$

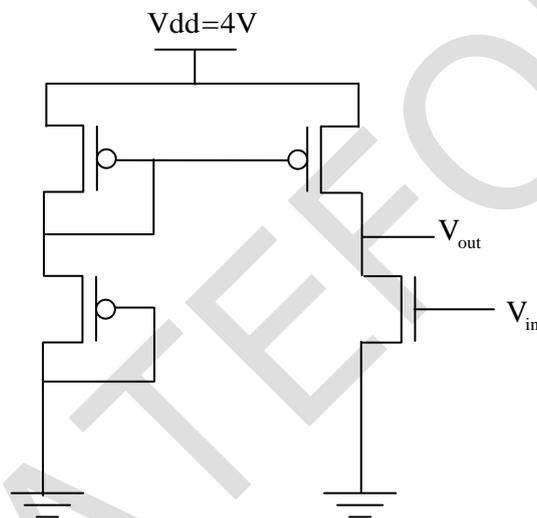
**Q. No. 26 - 55 Carry Two Marks Each**

26. In the circuit shown, the threshold voltages of the pMOS ( $|V_p|$ ) and nMOS ( $V_n$ ) transistors are both equal to 1 V. All the transistors have the same output resistance  $r_{ds}$  of  $6\text{ M}\Omega$ . The other parameters are listed below:

$$\mu_n C_{ox} = 60\mu\text{A}/\text{V}^2; \left(\frac{W}{L}\right)_{\text{nMOS}} = 5$$

$$\mu_p C_{ox} = 30\mu\text{A}/\text{V}^2; \left(\frac{W}{L}\right)_{\text{pMOS}} = 10$$

$\mu_n$  and  $\mu_p$  are the carrier mobilities, and  $C_{ox}$  is the oxide capacitance per unit area. Ignoring the effect of channel length modulation and body bias, the gain of the circuit is \_\_\_\_\_ (rounded off to 1 decimal place).



**Key: (-900)**

**Sol:**  $M_1$  and  $M_2$  will have equal current flowing also since they are identical  $\left(\frac{W}{L}\right)_1 = \left(\frac{W}{L}\right)_2$

$\therefore V_{SG_1} = V_{SG_2}$  also, By KVL in loop

$$4 = V_{SG_1} + V_{SG_2}$$

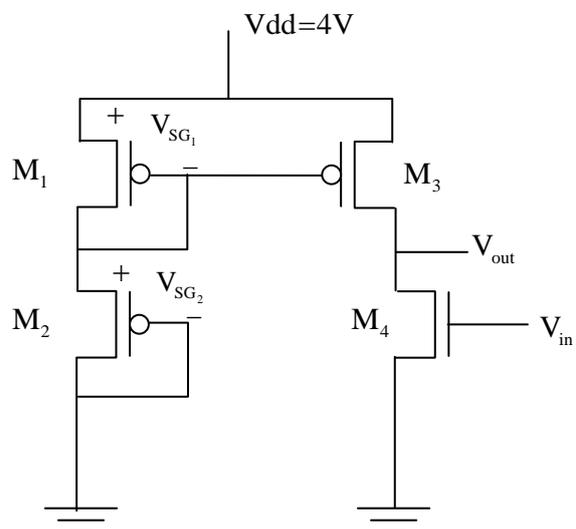
$$\therefore V_{SG_1} = V_{SG_2} = 2\text{V}$$

$\therefore$  current through  $M_1$  and  $M_2$

$$I = \left(\frac{1}{2}\right) (\mu_p C_{ox}) \left(\frac{W}{L}\right) [V_{SG} - |V_T|]^2$$

$$= \left(\frac{1}{2}\right) (30)(10)(2-1)^2 = 150\mu\text{A}$$

$M_1$  and  $M_3$  are matched with same



$\left(\frac{W}{L}\right)$  and same  $V_{SG}$  hence,

$$I_{M_3} = I_{M_4} = 150\mu A$$

For MOSFET  $M_4$ ,

$$g_m = \sqrt{2\mu_n C_{ox} \frac{W}{L} I_D}$$

$$= \sqrt{2 \times 60\mu \times 5 \times 150\mu} = 300\mu S$$

$$A_v = -g_m (r_d \parallel r_d) = \left(-300 \frac{\mu A}{V}\right) (6M\Omega \parallel 6M\Omega)$$

$$= \left(-300 \frac{\mu A}{V}\right) (3M\Omega) = -900 V/V$$

27. It is desired to find three-tap causal filter which gives zero signal as an output to an input of the form

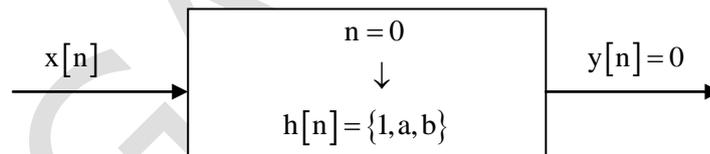
$$x[n] = c_1 \exp\left(-\frac{j\pi n}{2}\right) + c_2 \exp\left(\frac{j\pi n}{2}\right),$$

Where  $c_1$  and  $c_2$  are arbitrary real numbers. The desired three-tap filter is given by

$$h[0] = 1, \quad h[1] = a, \quad h[2] = b \text{ and}$$

$$h[n] = 0 \text{ for } n < 0 \text{ or } n > 2.$$

What are the values of the filter taps  $a$  and  $b$  if the output is  $y[n] = 0$  for all  $n$ , when  $x[n]$  is as given above?



(A)  $a = -1, b = 1$

(B)  $a = 0, b = 1$

(C)  $a = 1, b = 1$

(D)  $a = 0, b = -1$

**Key: (B)**

**Sol:** It is given that

$$h(n) = [1, a, b]$$

$$x(n) = C_1 e^{-j\frac{\pi}{2}n} + C_2 e^{j\frac{\pi}{2}n}$$

$$\Rightarrow y(n) = 0$$

$$\rightarrow \text{If } h(n) = [1, a, b]$$

$$H(e^{j\omega}) = 1 + ae^{-j\omega} + be^{-j2\omega}$$

→ when  $x(n) = C_1 e^{-j\frac{\pi}{2}n} + C_2 e^{j\frac{\pi}{2}n}$  then  
expression of  $y(n)$

Since the input  $x(n)$  contain 2 frequencies  $\pm \frac{\pi}{2}$ ,

Let evaluate  $|H(e^{j\omega})|$  at f nil 2 frequency

$$H(e^{j-\pi/2}) = 1 + ae^{-j(\frac{-\pi}{2})} + be^{-j2(\frac{-\pi}{2})}$$

$$= 1 + ae^{+j\pi/2} + be^{j\pi}$$

$$= 1 + [a(j)] + [b(-1)]$$

$$= (1-b) + j(a)$$

$$H(e^{j\pi/2}) = (1-b) - ja$$

$$|H(e^{j\pi/2})| = \left| H\left(e^{-j\frac{\pi}{2}}\right) \right| = \sqrt{(1-b)^2 + a^2}$$

So the expression of  $y(n)$  is

$$y(n) = \left[ (1-b)^2 + a^2 \right]^{1/2} C_1 e^{-j\left(\frac{1}{2}n + \phi_1\right)} + \left[ (1-b)^2 + a^2 \right]^{1/2} C_2 e^{j\left(\frac{\pi}{2}n + \phi_2\right)}$$

if we want  $y(n) = 0$ , it means

$$k = \sqrt{(1-b)^2 + a^2} = 0 \text{ (from the above expression)}$$

If we check each options

(A)  $a = -1, b = 1$ , then  $k = \sqrt{0^2 + 1^2} = 1$  (not correct)

(B)  $a = 0, b = 1$  then  $k = \sqrt{0^2 + 0^2} = 0$  (correct)

(C)  $a = 1, b = 1$ , then  $k = \sqrt{0^2 + 1^2} = 1$  (not correct)

(D)  $a = 0, b = 1$ , then  $k = \sqrt{2^2 + 0^2} = 2$  (not correct)

So  $a = 0, b = 1$ , is correct.

28. Let  $h[n]$  be length-7 discrete-time finite impulse response filter, given by

$$h[0] = 4, h[1] = 3, h[2] = 2, h[3] = 1$$

$$h[-1] = -3, h[-2] = -2, h[-3] = -1,$$

and  $h[n]$  is zero for  $|n| \geq 4$ . A length-3 finite impulse response approximation  $g[n]$  of  $h[n]$  has to be obtained such that

$$E(h, g) = \int_{-\pi}^{\pi} |H(e^{j\omega}) - G(e^{j\omega})|^2 d\omega$$

is minimized, where  $H(e^{j\omega})$  and  $G(e^{j\omega})$  are the discrete-time Fourier transforms of  $h[n]$  and  $g[n]$ , respectively. For the filter that minimizes  $E(h,g)$ , the value of  $10g[-1] + g[1]$ , rounded off to 2 decimal places, is \_\_\_\_\_.

**Key: (-27)**

**Sol:** It is given that

$$h(n) = [-1, -2, -3, 4, 3, 2, 1] \quad \dots(1)$$

And it is also mentioned that  $g(n)$  is derived from  $h(n)$  having 3 samples, from the information given in question we need  $g(1)$ , and  $g(-1)$  so left

$$g(n) = [a, b, c] \quad \dots(2)$$

It is mentioned that

$$E(h, g) = \int_{-\pi}^{\pi} |H(e^{j\omega}) - G(e^{j\omega})|^2 d\omega, \text{ is minimised,}$$

If  $h(n)$  and  $g(n)$  represent IDTFT of  $H(e^{j\omega})$ ,  $G(e^{j\omega})$

then  $E(h, g) = 2\pi \sum |h(n) - g(n)|^2$  (by Parseval theorem)

$$h(n) \leftrightarrow H(e^{j\omega})$$

$$g(n) \leftrightarrow G(e^{j\omega})$$

$$h(n) - g(n) \leftrightarrow H(e^{j\omega}) - G(e^{j\omega})$$

$$\text{energy of } [h(n) - g(n)] \leftrightarrow \frac{1}{2\pi} \int_{-\pi}^{\pi} |H(e^{j\omega}) - G(e^{j\omega})|^2 d\omega$$

$$\Rightarrow 2\pi \text{ energy of } [h(n) - g(n)] = \int_{-\pi}^{\pi} |H(e^{j\omega}) - G(e^{j\omega})|^2 d\omega$$

$$\Rightarrow E(h, g) = \int_{-\pi}^{\pi} |H(e^{j\omega}) - G(e^{j\omega})|^2 d\omega = 2\pi \sum_{n=-\infty}^{\infty} |h(n) - g(n)|^2$$

We want to minimize  $E(h, g)$

Using equation (1) and equation (2) we can say

$$h(n) - g(n) = [-1, -2, -3 - a, 4 - b, 3 - c, 2, 1]$$

$$\rightarrow E(h, g) = 2\pi \sum |h(n) - g(n)|^2 = 2\pi \sum [h(n) - g(n)]^2$$

[∵ all elements are real, mod does not have significance]

$$\rightarrow E(h, g) = 2\pi [(-1)^2 + (-2)^2 + (-3 - a)^2 + (4 - b)^2 + (3 - c)^2 + 2^2 + 1^2]$$

$$= 2\pi [10 + (-3 - a)^2 + (4 - b)^2 + (3 - c)^2]$$

To have minimum  $E(h, g)$ , we need

$$-3 - a = 0 \Rightarrow a = -3$$

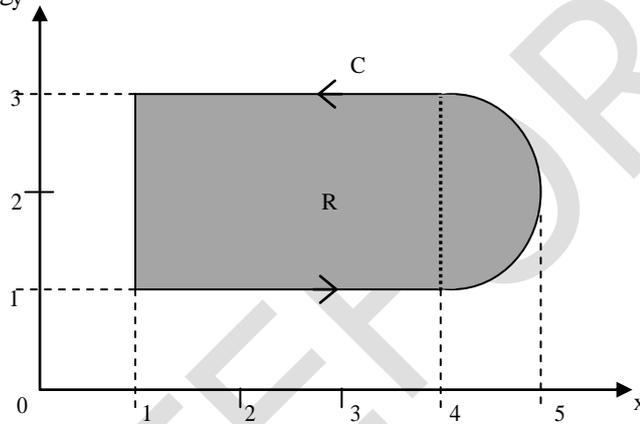
$$4 - b = 0 \Rightarrow b = 4$$

$$3 - c = 0 \Rightarrow c = 3$$

$$\rightarrow g(n) = [a, b, c] = [-3, 4, 3]$$

$$\text{So } 10g(-1) + g(1) = 10a + c = [10(-3)] + 3 = -30 + 3 = -27$$

29. Consider the line integral  $\int_C (x dy - y dx)$ . The integral being taken in a counterclockwise direction over the closed curve  $C$  that forms the boundary of the region  $R$  shown in the figure below. The region  $R$  is the area enclosed by the union of a  $2 \times 3$  rectangle and a semi-circle of radius 1. The line integral evaluates to



- (A)  $16 + 2\pi$       (B)  $6 + \pi/2$       (C)  $12 + \pi$       (D)  $8 + \pi$

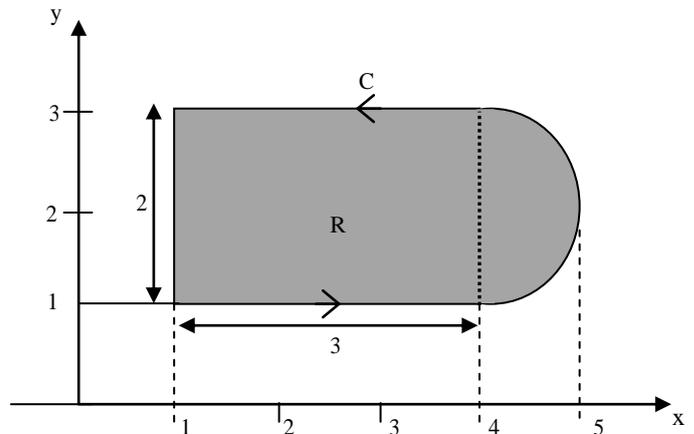
**Key: (C)**

**Sol:**  $\int_C (x dy - y dx) = \int_C (-y dx + x dy)$ ; where  $C$  is a

Closed figure formed by rectangle and a semi circle of radius 1.

Using Green's theorem, we have

$$\begin{aligned} \oint_C \left( \underset{\substack{\downarrow \\ M}}{-y} dx + \underset{\substack{\downarrow \\ N}}{x} dy \right) &= \iint_R (1+1) dx dy \\ &= 2 \iint_R dx dy \rightarrow \text{Area of the region R.} \\ &= 2 [\text{Area of rectangle} + \text{Area of semi-circle}] \\ &= 2 \left[ (3 \times 2) + \frac{1}{2} \pi (1^2) \right] \\ &= 2 [6 + \pi/2] = (12 + \pi) \end{aligned}$$



30. A rectangular waveguide of width  $w$  and height  $h$  has cut-off frequencies for  $TE_{10}$  and  $TE_{11}$  modes in the ratio 1:2. The aspect ratio  $w/h$ , rounded off to two decimal places, is \_\_\_\_\_.

**Key: (1.732)**

**Sol:** Cut off frequency of  $TE_{10}$  mode is  $f_{c_{10}} = \frac{C}{2W}$

Cutoff frequency of  $TE_{11}$  mode is  $f_{c_{11}} = \frac{C}{2W} \sqrt{1^2 + \left(\frac{W}{h}\right)^2}$

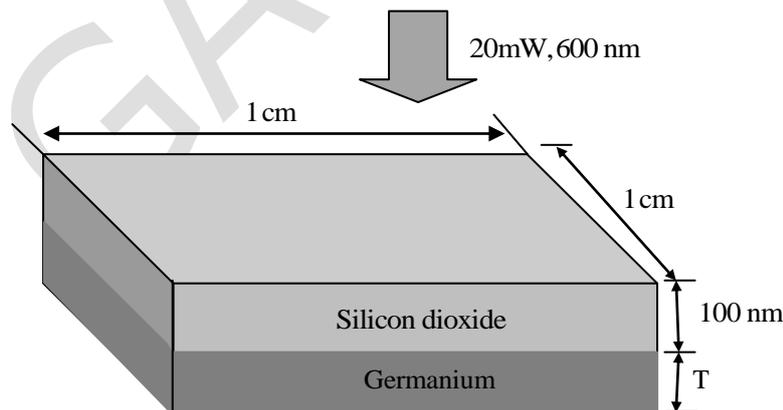
$$\text{Given } \frac{f_{c_{10}}}{f_{c_{11}}} = \frac{1}{2} \Rightarrow \frac{(C/2W)}{\left(\frac{C}{2W}\right) \sqrt{1^2 + \left(\frac{W}{h}\right)^2}} = \frac{1}{2}$$

$$\Rightarrow 1^2 + \left(\frac{W}{h}\right)^2 = 4$$

$$\Rightarrow \frac{W}{h} = \sqrt{3}$$

$$\therefore \text{Aspect ratio} = \frac{W}{h} = \sqrt{3} = 1.732.$$

31. A Germanium sample of dimensions  $1\text{cm} \times 1\text{cm}$  is illuminated with a  $20\text{ mW}$ ,  $600\text{ nm}$  laser light source as shown in the figure. The illuminated sample surface has a  $100\text{ nm}$  of loss-less Silicon dioxide layer that reflects one-fourth of the incident light. From the remaining light, one-third of the power is reflected from the silicon dioxide- Germanium interface, one-third is absorbed in the Germanium layer, and one-third is transmitted through the other side of the sample. If the absorption coefficient of Germanium at  $600\text{ nm}$  is  $3 \times 10^4\text{ cm}^{-1}$  and the bandgap is  $0.66\text{ eV}$ , the thickness of the Germanium layer, rounded off to 3 decimal places, is \_\_\_\_\_  $\mu\text{m}$ .



**Key: (0.231)**

**Sol:**  $0 \leftarrow P(0) = 10\text{mW}$

$T \leftarrow P(T) = 5\text{mW}$

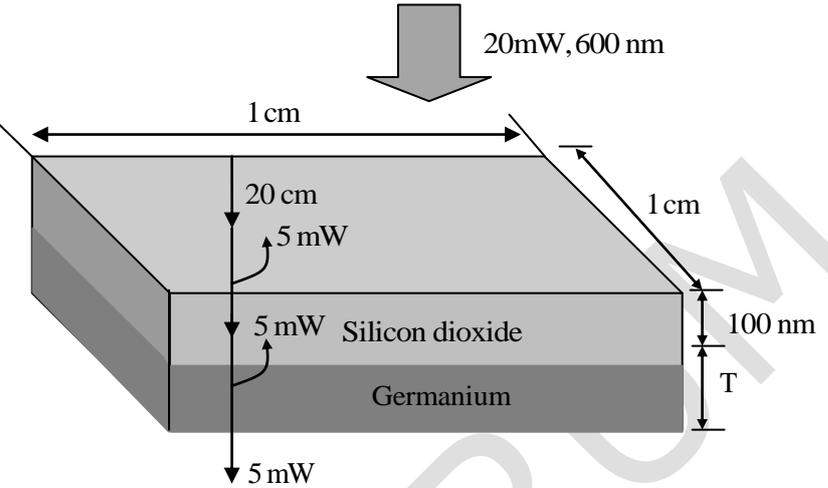
$\alpha = 3 \times 10^4 \text{cm}^{-1} = 3 \times 10^6 \text{m}^{-1}$

$P(T) = P(0)e^{-\alpha T}$

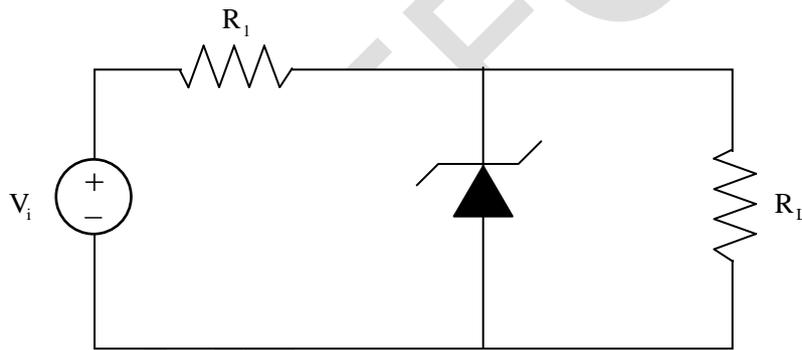
$T = \frac{1}{\alpha} \ln \left[ \frac{P(0)}{P(T)} \right]$

$T = \frac{1}{3 \times 10^6} \ln \left( \frac{10}{5} \right)$

$= 0.23 \times 10^{-6} \text{m} = 0.231 \mu\text{m}$



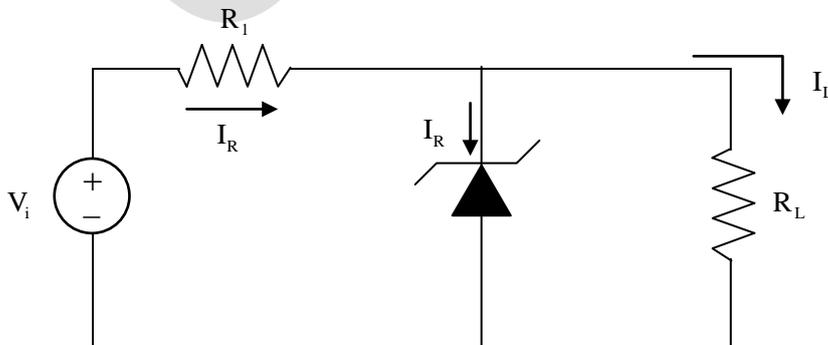
32. In the circuit shown, the breakdown voltage and the maximum current of the Zener diode are 20 V and 60 mA, respectively. The values of  $R_1$  and  $R_L$  are  $200 \Omega$  and  $1 \text{k}\Omega$ , respectively. What is the range of  $V_i$  that will maintain the Zener diode in the 'n' state?



- (A) 24 V to 36V      (B) 22 V to 34 V      (C) 20 V to 28 V      (D) 18 V to 24 V

**Key: (A)**

**Sol:**



$I_L = \frac{20 - 0}{1} \text{mA} = 20\text{mA}$

$$I_R = I_Z + I_L$$

$$V_{i\min} = I_{R\min} R_1 + V_Z$$

$$I_{R\min} = 0 + I_2 (\because I_{Z(\min)} = 0) = 20\text{mA}$$

$$V_{i\min} = 20 \times 10^{-3} \times 100 + 2 = 4\text{V} + 20\text{v} = 24\text{v}$$

$$V_{i\max} = I_{R\max} R_1 + V_Z$$

$$I_{R\max} = I_{Z\max} + I_L = 60\text{mA} + 20\text{mA} = 80\text{mA}$$

$$V_{i\max} = 80 \times 10^{-3} \times 200 + 20 = 16\text{V} + 20\text{V} = 36\text{V}$$

$$\therefore V_{i\min} = 24\text{V}; \quad V_{i\max} = 36\text{V}$$

33. A single bit, equally likely to be 0 and 1, is to be sent across an additive white Gaussian noise (AWGN) channel with power spectral density  $N_0/2$ . Binary signaling, with  $0 \rightarrow p(t)$  and  $1 \rightarrow q(t)$ , is used for the transmission, along with an optimal receiver that minimizes the bit-error probability.

Let  $\phi_1(t), \phi_2(t)$  form an orthonormal signal set.

If we choose  $p(t) = \phi_1(t)$  and  $q(t) = -\phi_1(t)$ , we would obtain a certain bit-error probability  $P_b$ .

If we keep  $p(t) = \phi_1(t)$ , but take  $q(t) = \sqrt{E}\phi_2(t)$ , for what value of  $E$  would we obtain the same bit-error probability  $P_b$ ?

(A) 3

(B) 1

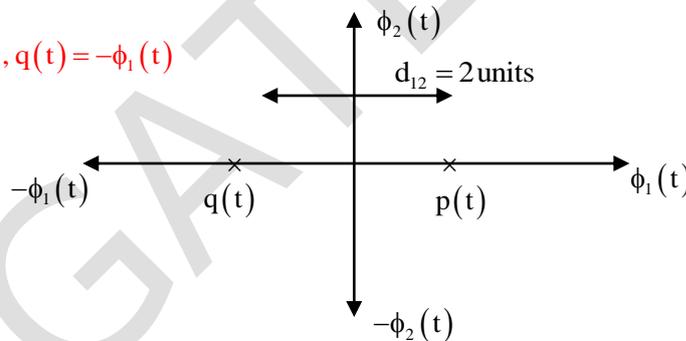
(C) 2

(D) 0

**Key: (A)**

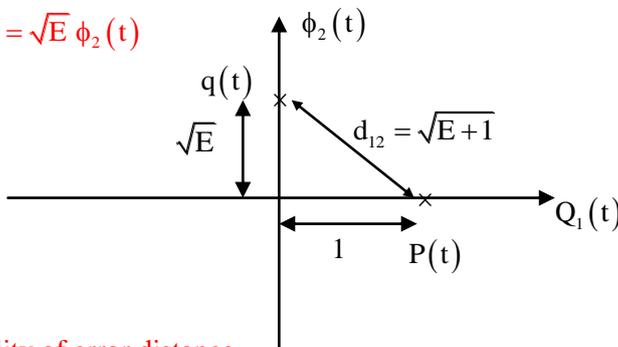
**Sol: Case 1:**

$$P(t) = \phi_1(t), \quad q(t) = -\phi_1(t)$$



**Case 2:**

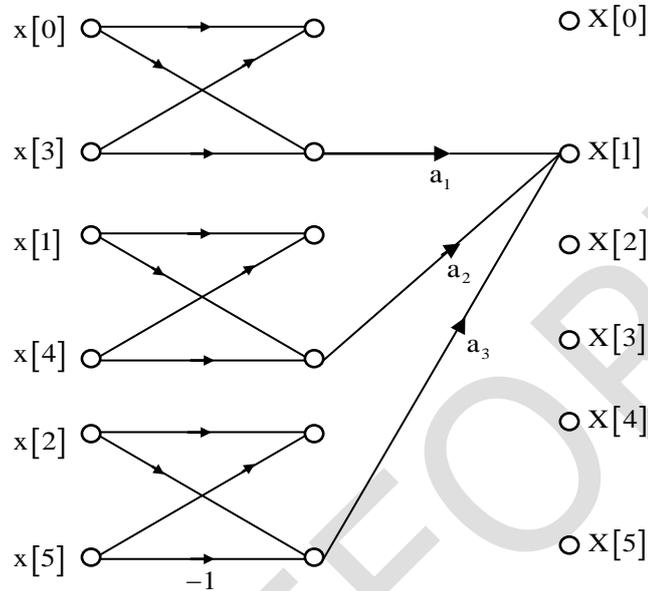
$$P(t) = \phi_1(t) \quad q(t) = \sqrt{E}\phi_2(t)$$



For same probability of error distance between points should be same for both cases

$$\therefore \sqrt{E+1} = 2 \quad \therefore E = 3$$

34. Consider a six-point decimation-in-time Fast Fourier Transform (FFT) algorithm, for which the signal-flow graph corresponding to  $X[1]$  is shown in the figure. Let  $W_6 = \exp\left(-\frac{j2\pi}{6}\right)$ . In the figure, what should be the values of the coefficients  $a_1, a_2, a_3$  in terms of  $W_6$  so that  $X[1]$  is obtained correctly ?



- (A)  $a_1 = 1, a_2 = W_6^2, a_3 = W_6$  (B)  $a_1 = -1, a_2 = W_6^2, a_3 = W_6$   
 (C)  $a_1 = -1, a_2 = W_6, a_3 = W_6^2$  (D)  $a_1 = 1, a_2 = W_6, a_3 = W_6^2$

**Key: (D)**

**Sol:** In this case we are supposed to obtain the FFT coefficient  $[X(1)]$  using DIT algorithm.

We are supposed to obtain the coefficient  $a_1, a_2, a_3$

The given butterfly structure is a standard structure where

$$a_1 = W_6^0 = 1$$

$$a_2 = W_6^1 = W_6$$

$$a_3 = W_6^2$$

35. The quantum efficiency ( $\eta$ ) and responsivity ( $R$ ) at a wavelength  $\lambda$  (in  $\mu\text{m}$ ) in a p-i-n photo detector are related by

- (A)  $R = \frac{\eta \times \lambda}{1.24}$  (B)  $R = \frac{\lambda}{\eta \times 1.24}$  (C)  $R = \frac{1.24 \times \lambda}{\eta}$  (D)  $R = \frac{1.24}{\eta \times \lambda}$

**Key: (A)**

**Sol:** Responsivity ( $R$ ) =  $\frac{e\eta}{h\nu} = \frac{e\eta s}{hc} = \frac{\eta \times \lambda}{1.24} \text{ (A/w)}$

36. Consider a long-channel MOSFET with a channel length  $1\mu\text{m}$  and width  $10\mu\text{m}$ . The device parameters are acceptor concentration  $N_A = 5 \times 10^{16} \text{ cm}^{-3}$ , electron mobility  $\mu_n = 800 \text{ cm}^2/\text{V-s}$ , oxide capacitance/area  $C_{ox} = 3.45 \times 10^{-7} \text{ F/cm}^2$ , threshold voltage  $V_T = 0.7\text{V}$ . The drain saturation current ( $I_{Dsat}$ ) for a gate voltage of  $5\text{V}$  is \_\_\_\_\_mA (rounded off to two decimal places).  $[\epsilon_0 = 8.854 \times 10^{-14} \text{ F/cm}, \epsilon_{si} = 11.9]$

**Key: (25.51)**

**Sol:** Given data;  $L = 1\mu\text{m}, W = 10\mu\text{m}$

$$N_A = 5 \times 10^{16} \text{ cm}^{-3}, \mu_n = 800 \frac{\text{cm}^2}{\text{v-sec}}$$

$$C_{ox} = 3.45 \times 10^{-7} \text{ F/cm}, V_T = 0.7\text{V}$$

$$\epsilon_0 = 8.854 \times 10^{-14} \text{ F/cm}, \epsilon_{si} = 11.9$$

$$V_G = 5\text{V}$$

$$I_{Dsat} = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} [V_G - V_T]^2$$

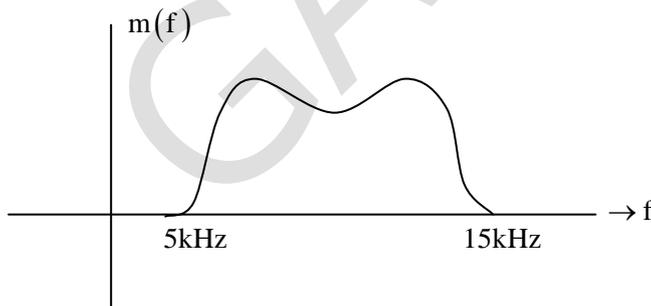
$$= \frac{1}{2} \times 800 \times 3.45 \times 10^{-7} \times \frac{10}{1} [5 - 0.7]^2 = 0.0255\text{A} = 25.5162 \text{ mA} \approx 25.51\text{mA}$$

37. A voice signal  $m(t)$  is in the frequency range  $5 \text{ kHz}$  to  $15 \text{ kHz}$ . The signal is amplitude modulated to generate an AM signal  $f(t) = A(1 + m(t))\cos 2\pi f_c t$ , where  $f_c = 600 \text{ kHz}$ .

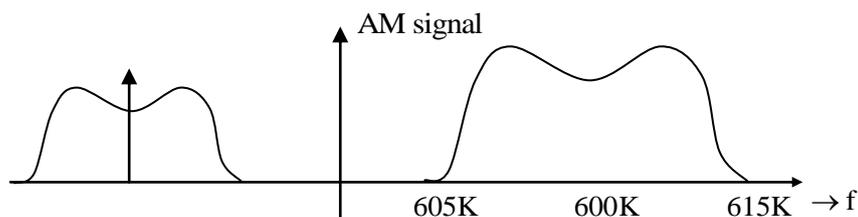
The Am signal  $f(t)$  is to be digitized and archived. This is done by first sampling  $f(t)$  at 1.2 times the Nyquist frequency, and then quantizing each sample using a 256-level quantizer. Finally, each quantized sample is binary coded using  $K$  bits, where  $K$  is the minimum number of bits required for the encoding. The rate, in Megabits per second (rounded off to 2 decimal places), of the resulting stream of coded bits is \_\_\_\_\_Mbps.

**Key: (0.192)**

**Sol:**



**Modulation done using AM**



Now AM signal is done sampling

$$\frac{2f_{+1}}{n} \leq f_s \leq \frac{2f_{-1}}{n-1}$$

Here  $f_H = 615\text{K}$ ,  $f_L = 605\text{K}$ .

$$1 \leq n \leq \frac{f_H}{B} : B = f_H - f_L$$

$$n \leq 61.5, n = 61.$$

$$f_s \geq \frac{2 \times 615}{61}$$

Minimum sampling is 20 K.

$$R_b = 1.2f_s \times 8 = 0.192\text{M bit/s}$$

38. A random variable  $X$  takes values  $-1$  and  $+1$  with probabilities  $0.2$  and  $0.8$ , respectively. It is transmitted across a channel which adds noise  $N$ , so that the random variable at the channel output is  $Y = X + N$ . The noise  $N$  is independent of  $X$ , and is uniformly distributed over the interval  $[-2, 2]$ . The receiver makes a decision

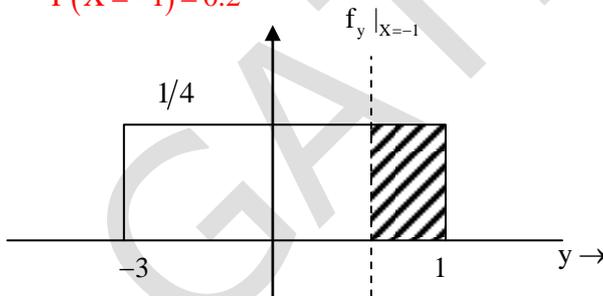
$$X = \begin{cases} -1, & \text{if } Y \leq \theta \\ +1, & \text{if } Y > \theta \end{cases}$$

Where the threshold  $\theta \in [-1, 1]$  is chosen so as to minimize the probability of error  $\Pr[X \neq \hat{X}]$ .

The minimum probability of error, rounded off to 1 decimal place, is \_\_\_\_\_.

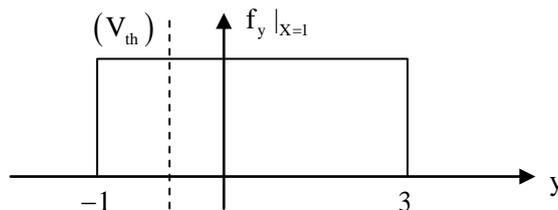
**Key: (0.1)**

**Sol:** When  $X = -1$  is transmitted  
 $P(X = -1) = 0.2$



$$P_{e,-1} = (0.2) \left( \frac{1}{4} \right) (1 - V_{th})$$

When  $X = 1$  is transmitted  $P[X = 1] = 0.8$



$$P_{e_1} = (0.8) \left( \frac{1}{4} \right) (V_{th} + 1)$$

$$P_e = \frac{(0.2)(1)(1 - V_{th}) + (0.8)(1)(V_{th} + 1)}{4}$$

$$P_e = \frac{1 + 0.6V_{th}}{4}$$

$$-1 \leq V_{th} \leq 1$$

$$\therefore P_{e_{min}} \text{ when } V_{th} = -1$$

$$\therefore P_{e_{min}} = \frac{1 + (0.6)(-1)}{4} = \frac{0.4}{4} = 0.1$$

39. Let the state-space representation of an LTI system be  $\dot{x}(t) = Ax(t) + Bu(t)$ ,  $y(t) = Cx(t) + d u(t)$  where A,B,C are matrices, d is a scalar, u(t) is the input to the system, and y(t) is its output. Let  $B = [0 \ 0 \ 1]^T$  and  $d = 0$ . Which one of the following options for A and C will ensure that the transfer function of this LTI system is  $H(s) = \frac{1}{s^3 + 3s^2 + 2s + 1}$ ?

(A)  $A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -2 & -3 \end{bmatrix}$  and  $C = [1 \ 0 \ 0]$

(B)  $A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -2 & -3 \end{bmatrix}$  and  $C = [0 \ 0 \ 1]$

(C)  $A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -3 & -2 & -1 \end{bmatrix}$  and  $C = [0 \ 0 \ 1]$

(D)  $A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -3 & -2 & -1 \end{bmatrix}$  and  $C = [1 \ 0 \ 0]$

**Key:** (A)

**Exp:**  $H(s) = \frac{1}{s^3 + 3s^2 + 2s + 1}$

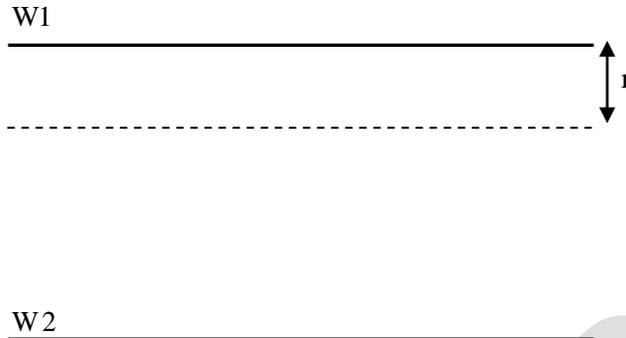
$$\begin{bmatrix} \dot{X}_1 \\ \dot{X}_2 \\ \dot{X}_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -2 & -3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} u$$

$$y = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

(C matrix)

(A matrix)

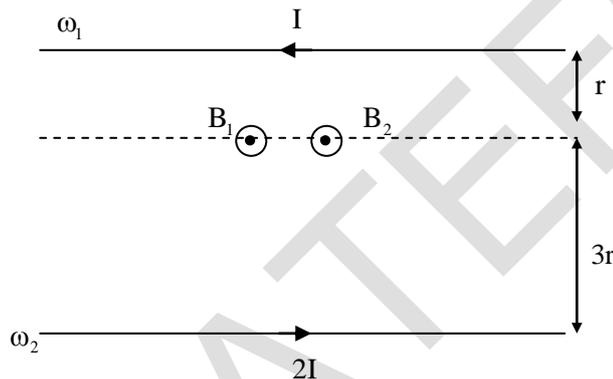
40. Two identical copper wires W1 and W2, placed in parallel as shown in the figure, carry currents I and 2I, respectively, in opposite directions. If the two wires are separated by a distance of 4r, then the magnitude of the magnetic field  $\vec{B}$  between the wires at a distance r from W1 is



- (A)  $\frac{5\mu_0 I}{6\pi r}$       (B)  $\frac{\mu_0 I}{6\pi r}$       (C)  $\frac{6\mu_0 I}{5\pi r}$       (D)  $\frac{\mu_0 I^2}{2\pi r^2}$

**Key: (A)**

**Sol:**



Between the wires  $\omega_1$  and  $\omega_2$  the  $\vec{B}$  - fields due to I and 2I will get added up.

∴ The B - field due to  $\omega_1$  at a distance 'r' from the  $\omega_1$  is  $B_1 = \frac{\mu_0 I}{2\pi r} \rightarrow (1)$

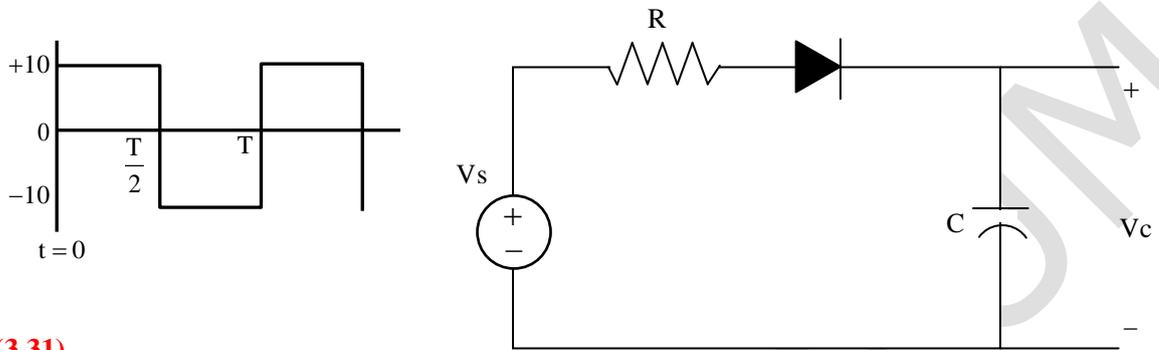
The B - field due to  $\omega_2$  at a distance "3r" from the  $\omega_2$  as shown in figure is  $B_2 = \frac{\mu_0 (2I)}{2\pi (3r)} \rightarrow (2)$

∴ The total B - field  $B = B_1 + B_2$

$$= \frac{\mu_0 I}{2\pi} \left[ \frac{1}{r} + \frac{2}{3r} \right]$$

$$B = \frac{5\mu_0 I}{6\pi r} \text{ wb/m}^2.$$

41. In the circuit shown,  $V_s$  is a 10V square wave of period,  $T=4$  ms with  $R = 500\Omega$  and  $C = 10\mu\text{F}$ . The capacitor is initially uncharged at  $t = 0$ , and the diode is assumed to be ideal. The voltage across the capacitor ( $V_c$ ) at 3 ms is equal to \_\_\_\_\_ volts (rounded off to one decimal place).

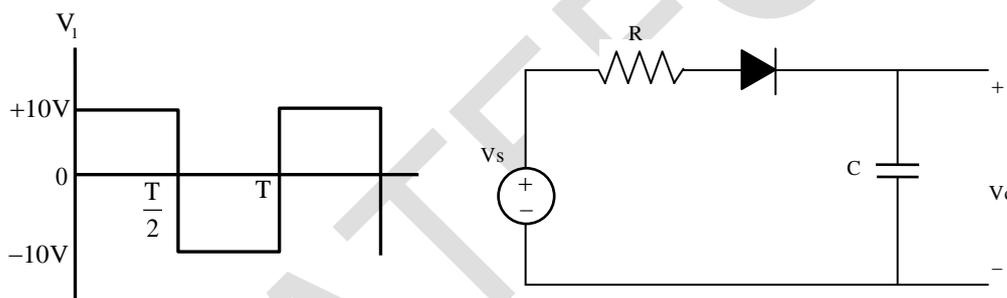


**Key: (3.31)**

**Sol:** Given:  $T = 4\text{ms}$ ,  $R = 500\Omega$ ,  $C = 10\mu\text{F}$

$$\tau = RC = 500 \times 10 \times 10^{-6} \text{ sec} = 5\text{ms}$$

$$\frac{T}{2} = \frac{4\text{ms}}{2} = 2\text{ms}$$



For positive half cycle, diode will be forward biased and capacitor start to charge

$$V_c = V_c(\infty) \left[ 1 - e^{-\frac{t}{RC}} \right] = 10 \left[ 1 - e^{-\frac{2\text{ms}}{5\text{ms}}} \right]$$

$$= 10 \left[ 1 - e^{-\frac{2}{5}} \right] = 4.51\text{V} \Rightarrow \therefore V_c = 3.31\text{V}$$

42. Consider a causal second-order system with the transfer function  $G(s) = \frac{1}{1 + 2s + s^2}$

With a unit-step  $R(s) = \frac{1}{s}$  as an input. Let  $C(s)$  be the corresponding output. The time taken by the system output  $C(t)$  to reach 94% of its steady-state value  $\lim_{t \rightarrow \infty} C(t)$ , rounded off to two decimal places, is

- (A) 5.25                      (B) 2.81                      (C) 4.50                      (D) 3.89

**Key: (C)**

**Sol:** Given,  $G(s) = \frac{1}{1+2s+s^2}$

$$\therefore C(s) = G(s) R(s) = \frac{1}{s(s+1)^2}$$

$$C(t) = 1 - e^{-t} - te^{-t}$$

Let's check option one by one

Option (A)

$$0.94 = 1 - e^{-5.25} - 5.25 e^{-5.25} = 0.89$$

(Hence option A is wrong)

Option (C)

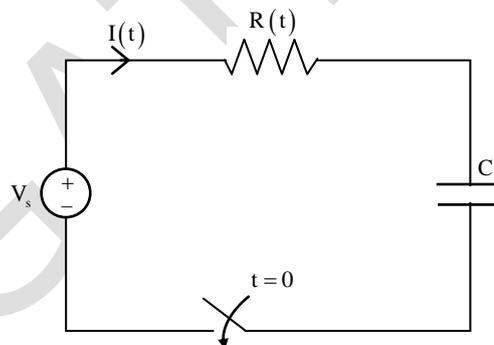
$$0.94 = 1 - e^{-4.50} - 4.50 e^{-4.50} = 0.94$$

(Hence option (C) is correct)

43. The RC circuit shown below has a variable resistance  $R(t)$  given by the following expression:

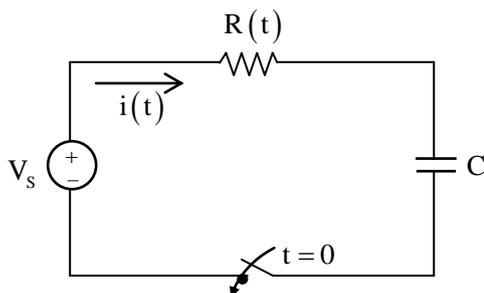
$$R(t) = R_0 \left( t - \frac{t}{T} \right) \text{ for } 0 \leq t < T$$

Where  $R_0 = 1\Omega$ ,  $C = 1F$ . We are also given that  $T = 3 R_0 C$  and the source voltage is  $V_s = 1V$ . If the current at time  $t = 0$  is  $1A$ , then the current  $I(t)$ , in amperes, at time  $t = T/2$  is \_\_\_\_\_ (rounded off to 2 decimal places).



**Key: (0.25)**

**Exp:** The given circuit is as shown in figure



Where  $R(t) = R_0 \left(1 - \frac{t}{T}\right)$  for  $0 \leq t \leq T$

and  $(R_0 = 1\Omega), (C = 1F), (T = 3R_0C), (V_s = 1V), (i(0) = 1A)$

We need to obtain  $i(t)$  at  $t = \frac{T}{2}$

$$\left[ \begin{array}{l} T = 3 (\because R_0 = 1\Omega, C = 1F) \\ R(t) = \left(1 - \frac{t}{3}\right) \\ \frac{T}{2} = 1.5 \end{array} \right]$$

By KVL we have

$$i(t)R(t) + \frac{1}{C} \int i dt = V_s$$

$$\Rightarrow R(t) \frac{di(t)}{dt} + i(t) \frac{dR(t)}{dt} + \frac{1}{C} i = 0$$

$$\Rightarrow \left(1 - \frac{t}{3}\right) \frac{di(t)}{dt} + i(t) \left(\frac{-1}{3}\right) + i = 0$$

$$\Rightarrow (3-t) \frac{di}{dt} = -2i$$

$$\Rightarrow \frac{di}{i} = \frac{-2}{3-t} dt$$

$$\Rightarrow \ln i = 2 \ln(t-3) + \ln C$$

$$\Rightarrow \ln i = \ln \left[ (t-3)^2 \cdot C \right]$$

$$\Rightarrow i(t) = (t-3)^2 C$$

$$\Rightarrow i(0) = (0-3)^2 C$$

$$\Rightarrow C = \frac{1}{9} (\because i(0) = 1, \text{ given})$$

$$i(t) = (t-3)^2 \frac{1}{9}$$

$$i(1.5) = \frac{1}{9} (-1.5)^2 = 0.25A$$

44. In an ideal p-n junction with an ideality factor of 1 at  $T=300$  K, the magnitude of the reverse-bias voltage required to reach 75% of its reverse saturation current, rounded off to 2 decimal places, is \_\_\_\_\_ mV.

$$[k = 1.38 \times 10^{-23} \text{ JK}^{-1}, h = 6.625 \times 10^{-34} \text{ J-s}, q = 1.602 \times 10^{-19} \text{ C}]$$

**Key: (35.87)**

$$\text{Sol: } I = I_0 \left[ \exp\left(\frac{-V_R}{V_T}\right) - 1 \right] = \frac{-3}{4} I_0 = I_0 \left[ \exp\left(\frac{-V_R}{V_T}\right) - 1 \right]$$

$$\exp\left[\frac{-V_R}{V_T}\right] = \frac{-3}{4} + 1 = \frac{1}{4}$$

$$-V_R = V_T \ln\left(\frac{1}{4}\right) = 25.9 \times \ln\left(\frac{1}{4}\right) \text{ mV}$$

$$|-V_R| = 35.87 \text{ mV}$$

45. The dispersion equation of a waveguide, which relates the wave number  $k$  to the frequency  $\omega$ , is

$$k(\omega) = (1/c) \sqrt{\omega^2 - \omega_0^2}$$

Where the speed of light  $c = 3 \times 10^8$  m/s, and  $\omega_0$  is a constant. If the group velocity is  $2 \times 10^8$  m/s, then the phase velocity is

- (A)  $2 \times 10^8$  m/s      (B)  $1.5 \times 10^8$  m/s      (C)  $3 \times 10^8$  m/s      (D)  $4.5 \times 10^8$  m/s

**Key: (D)**

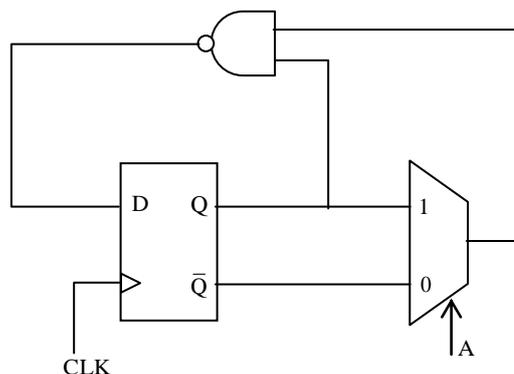
**Sol:** Given,  $C = 3 \times 10^8$  m/sec

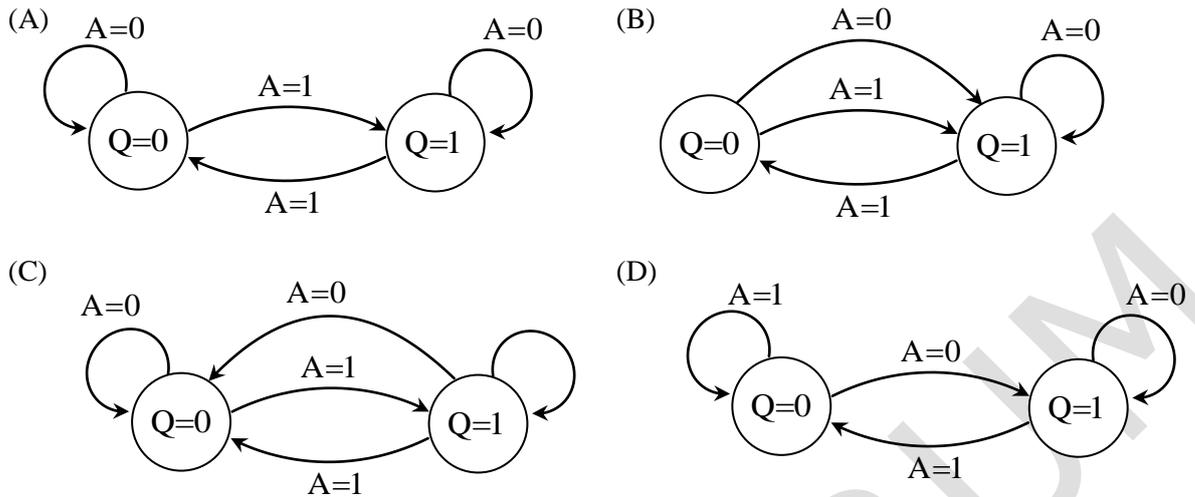
Group velocity  $v_g = 2 \times 10^8$  m/sec

$$v_p v_g = C^2$$

$$\therefore \text{Phase velocity } v_p = \frac{C^2}{v_g} = \frac{(3 \times 10^8)^2}{2 \times 10^8} = 4.5 \times 10^8 \text{ m/sec}$$

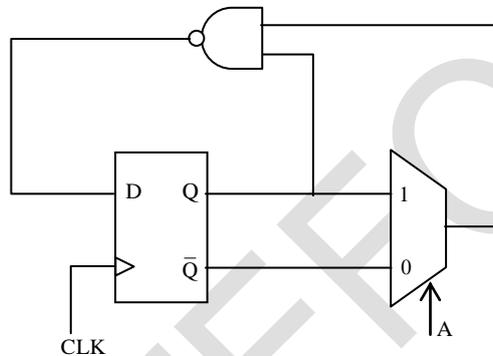
46. The state transition diagram for the circuit shown is





**Key: (B)**

**Sol:** The given circuit is



Let  $Q = 0$

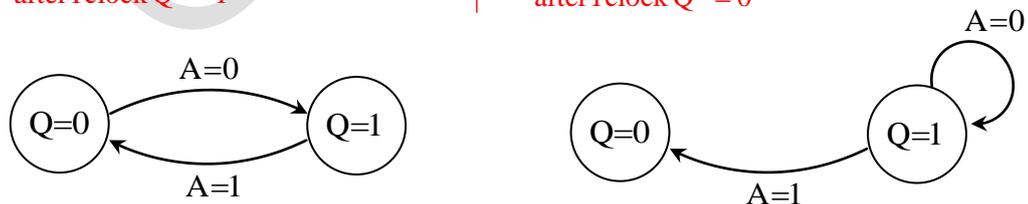
→ When  $Q = 0, \bar{Q} = 1$  and  $A = 0$ ,  
then  $Y = \bar{Q} = 1$ , so  $D = \overline{QY} = \overline{0.1} = \overline{0} = 1$   
after 1 clock  $Q^+ = 1$

→ When  $Q = 0, \bar{Q} = 1$  and  $A = 1$ ,  
then  $Y = Q = 1$ , so  $D = \overline{QY} = \overline{0.0} = \overline{0} = 1$   
after 1 clock  $Q^+ = 1$

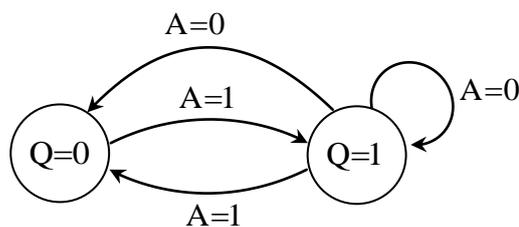
Let  $Q = 1$

→ When  $Q = 1, \bar{Q} = 0$  and  $A = 0$ ,  
then  $Y = \bar{Q} = 0$ , so  $D = \overline{QY} = \overline{1.0} = \overline{0} = 1$   
after 1 clock  $Q^+ = 1$

→ When  $Q = 1, \bar{Q} = 0$  and  $A = 1$ ,  
then  $Y = Q = 1$ , so  $D = \overline{QY} = \overline{1.1} = \overline{1} = 0$   
after 1 clock  $Q^+ = 0$



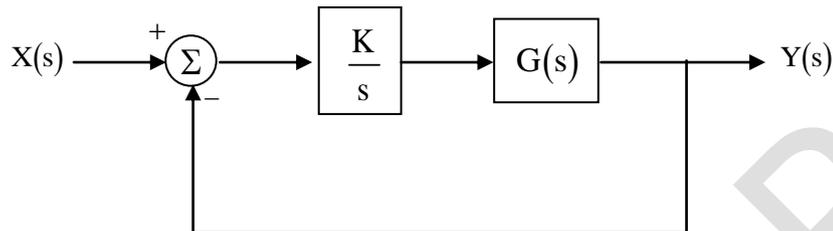
By combining both we can draw a single state diagram



47. Consider a unity feedback system, as in the figure shown, with an integral compensator  $\frac{k}{s}$  and open-loop transfer function

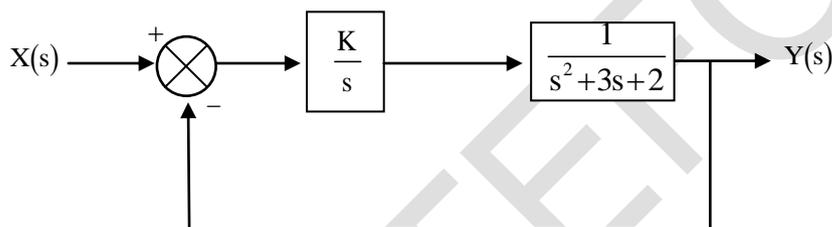
$$G(s) = \frac{1}{s^2 + 3s + 2}$$

Where  $K > 0$ . The positive value of  $K$  for which there are exactly two poles of the unity feedback system on the  $j\omega$  axis is equal to \_\_\_\_\_ (rounded off to two decimal places).



**Key: (6)**

**Sol:** Given, A unity feedback system as shown in figure



$$CE = s(s^2 + 3s + 2) + k = 0$$

$$\Rightarrow s^3 + 3s^2 + 2 + k = 0$$

$$\begin{array}{l|ll} s^3 & 1 & 2 \\ s^2 & 3 & k \\ s^1 & \frac{6-k}{3} & 0 \\ s^0 & k & 0 \end{array}$$

If this row will be zero then two poles will be on  $j\omega$  axis

$$6 - K = 0 \Rightarrow \boxed{K = 6}$$

Lets cross check :  $3s^2 + 6 = 0 \Rightarrow s^2 + 2 = 0$

$$\boxed{s = \pm j2}$$

Two poles on  $j\omega$

48. Consider a differentiable function  $f(x)$  on the set of real numbers such that  $f(-1)=0$  and  $|f'(x)| \leq 2$ . Given these conditions, which one of the following inequalities is necessarily true for all  $x \in [-2, 2]$  ?

- (A)  $f(x) \leq 2|x+1|$       (B)  $f(x) \leq 2|x|$       (C)  $f(x) \leq \frac{1}{2}|x+1|$       (D)  $f(x) \leq \frac{1}{2}|x|$

**Key: (A)**

**Sol: Method-I:**

Option (A) satisfy the given conditions ( $f(-1)=0$  &  $|f'(x)| \leq 2$ )

**Method-II:**

Given that  $|f'(x)| \leq 2$ ;  $f(-1)=0$

$\Rightarrow -2 \leq f'(x) \leq 2$ ; where  $x \in [-2, 2]$

Using Lagrange's Mean Value Theorem over  $[-1, 2]$ , we have

$$\Rightarrow -2 \leq f'(x) \leq 2 \Rightarrow -2 \leq \frac{f(2)-f(-1)}{2-(-1)} \leq 2 \quad \left[ \because f'(c) = \frac{f(b)-f(a)}{b-a} \right]$$

$$\Rightarrow -2 \leq \frac{f(2)-0}{3} \leq 2$$

$$\Rightarrow -6 \leq f(2) \leq 6 \quad \dots(2)$$

$\therefore$  Option (A) satisfies equation (2).

49. Consider the homogeneous ordinary differential equation  $x^2 \frac{d^2y}{dx^2} - 3x \frac{dy}{dx} + 3y = 0$ ,  $x > 0$

With  $y(x)$  as a general solution. Given that  $y(1)=1$  and  $y(2)=14$  the value of  $y(1.5)$ , (rounded off to two decimal places), is \_\_\_\_\_.

**Key: (5.25)**

**Sol:** Given D.E

$$x^2 \frac{d^2y}{dx^2} - 3x \frac{dy}{dx} + 3y = 0, \quad \dots(1)$$

$$x > 0 \text{ \& } y(1)=1 \text{ and } y(2)=14$$

Clearly equation(1) is Cauchy-Euler Linear Differential Equation.

Equation (1) can be written as

$$\left[ x^2 D^2 - 3xD + 3 \right] y = 0$$

Let  $x D = \theta$ ;  $x^2 D^2 = \theta(\theta - 1)$ ; where  $\theta = \frac{d}{dz}$  and  $x = e^z$

$$\therefore [\theta(\theta - 1) - 3\theta + 3] y = 0 \Rightarrow [\theta^2 - 4\theta + 3] y = 0$$

Consider the A.E is  $\theta^2 - 4\theta + 3 = 0 \Rightarrow (\theta - 3)(\theta - 1) = 0$

$\Rightarrow \theta = 1, 3 \rightarrow$  Roots are real & distinct

$\therefore$  The solution is,  $y = C_1 e^{1 \cdot z} + C_2 e^{3 \cdot z} \Rightarrow y = C_1 x + C_2 x^3$  ... (2)

$$[\because x = e^z]$$

Given,  $y = 1$  at  $x = 1 \Rightarrow 1 = C_1 + C_2$  ( $\because$  (2)) ... (3)

&  $y = 14$  at  $x = 2 \Rightarrow 14 = 2C_1 + 8C_2$  [ $\because$  (2)]

$$\Rightarrow C_1 + 4C_2 = 7 \dots (4)$$

Solving (3) and (4), we have

$$C_1 + C_2 = 1$$

$$C_1 + 4C_2 = 7$$

$$\underline{-3C_2 = -6} \Rightarrow C_2 = 2 \therefore C_1 = -1$$

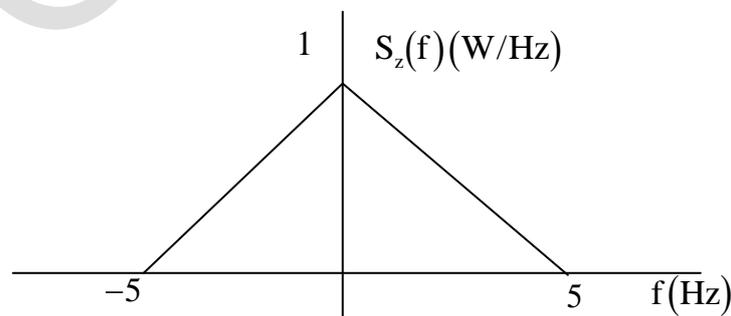
From (2),

$$y = (-1)x + (2)x^3$$

$$\Rightarrow y(1.5) = (-1)(1.5) + 2(1.5)^3$$

$$\Rightarrow y(1.5) = 5.25$$

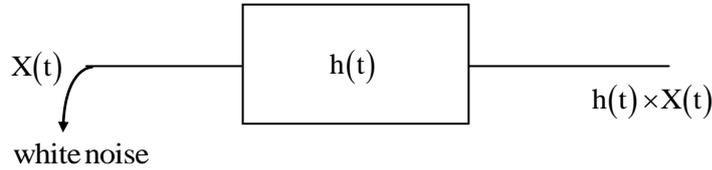
50. Let a random process  $Y(t)$  be described as  $Y(t) = h(t) \times X(t) + Z(t)$ , where  $X(t)$  is a white noise process with power spectral density  $S_x(f) = 5 \text{ W/Hz}$ . The filter  $h(t)$  has a magnitude response given by  $|H(f)| = 0.5$  for  $-5 \leq f \leq 5$ , and zero elsewhere.  $Z(t)$  is a stationary random process, uncorrelated with  $X(t)$ , with power spectral density as shown in the figure.



The power in  $Y(t)$ , in watts, is equal to \_\_\_\_\_ W. (rounded off to two decimal places).

**Key: (17.5)**

**Sol:** Power in  $y(t) = \left[ \text{Power in } h(t) \times X(t) \right] + \left[ \text{Power in } Z(t) \right]$   
( $Z(t)$  &  $X(t)$  uncorrelated)

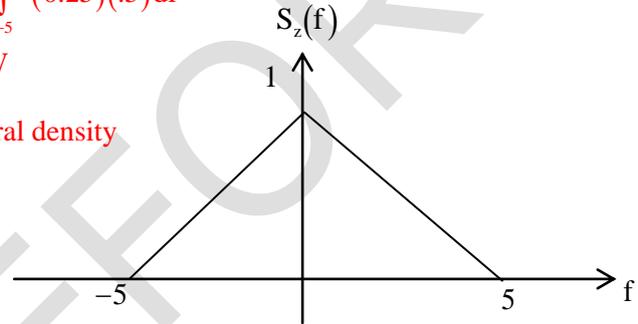


$$\begin{aligned} \text{Power in } h(t) \times X(t) &= \int_{-\infty}^{\infty} |H(f)|^2 S_{xx}(f) df \\ &= \int_{-\infty}^{\infty} |H(f)|^2 (5) df = \int_{-5}^5 (0.25)(5) df \\ &= (10)(1.25) = 12.5W \end{aligned}$$

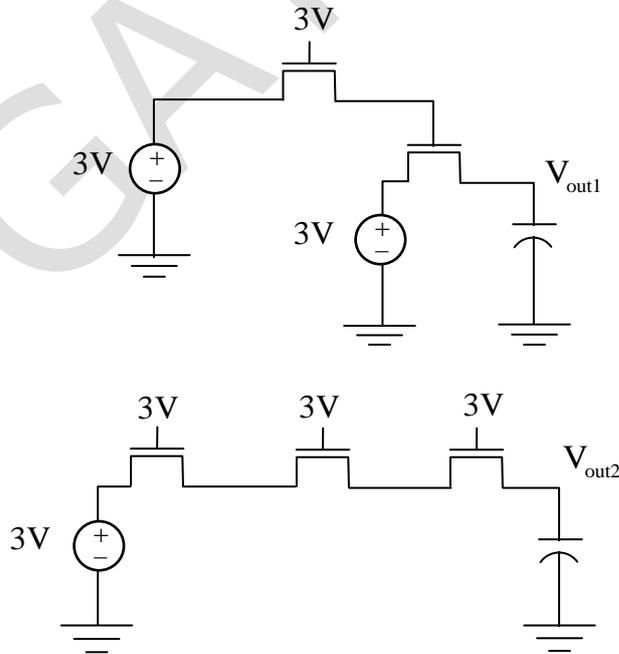
Power in  $S_z(f) = \text{Area under power spectral density}$

$$P_{z(t)} = \left( \frac{1}{2} \right) (10)(1) = 5W$$

$$\therefore \text{Power in } y(t) = 12.5 + 5 = 17.5W$$



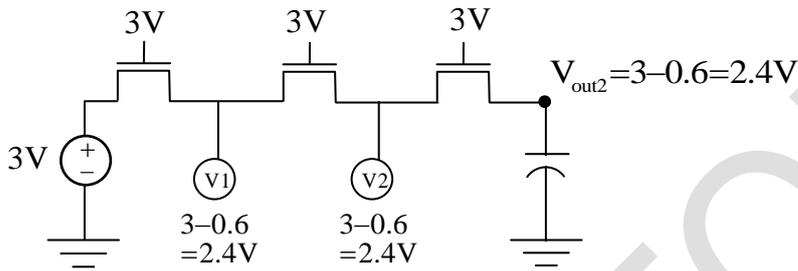
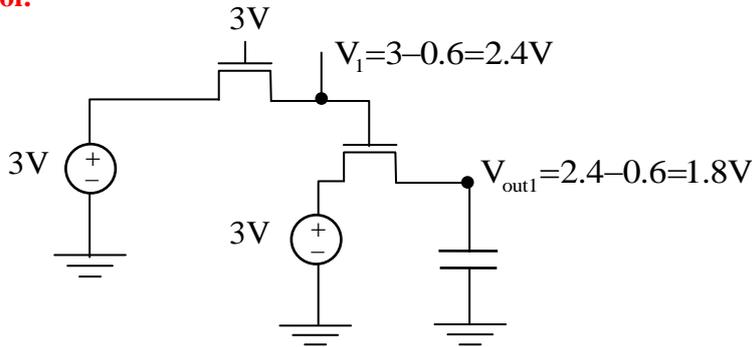
51. In the circuits shown, the threshold voltage of each nMOS transistor is 0.6V. Ignoring the effect of channel length modulation and body bias, the values of  $V_{out1}$  and  $V_{out2}$ , respectively, in volts, are



- (A) 2.4 and 1.2      (B) 2.4 and 2.4      (C) 1.8 and 1.2      (D) 1.8 and 2.4

**Key: (D)**

**Sol:**

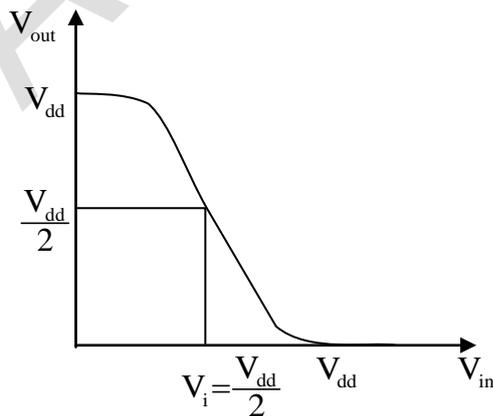


52. A CMOS inverter, designed to have a mid-point voltage  $V_i$  equal to half of  $V_{dd}$ , as shown in the figure, has the following parameters:

$$V_{dd} = 3V$$

$$\mu_n C_{ox} = 100\mu A/V^2; V_{tn} = 0.7V \text{ for nMOS}$$

$$\mu_p C_{ox} = 40\mu A/V^2; |V_{tp}| = 0.9V \text{ for pMOS}$$

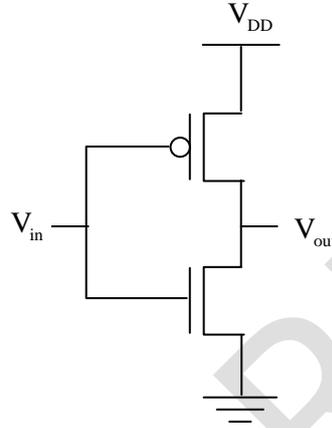


The ratio of  $\left(\frac{W}{L}\right)_n$  to  $\left(\frac{W}{L}\right)_p$  is equal to \_\_\_\_\_. (rounded off to three decimal places).

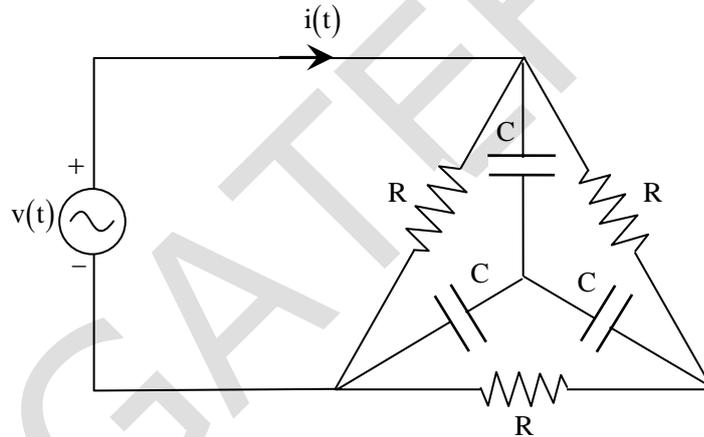
**Key: (0.225)**

**Sol:** At  $V_i = \frac{V_{DD}}{2}$ , both the MOSFETs are in saturation and both MOSFETs have the same current.

$$\begin{aligned} & \left( \frac{V_{dd}}{2} \right) \\ \therefore & \left( \frac{1}{2} \right) (100 \mu A / V^2) \left( \frac{W}{L} \right)_n [1.5 - 0.7]^2 \\ & = \left( \frac{1}{2} \right) (40 \mu A / V^2) \left( \frac{W}{L} \right)_p (3 - 1.5 - 0.9)^2 \\ \left( \frac{W}{L} \right)_n & = \frac{(40)(0.6)^2}{\left( \frac{W}{L} \right)_p (100)(0.8)^2} = 0.225 \end{aligned}$$



53. In the circuit shown, if  $v(t) = 2\sin(1000t)$  volts,  $R = 1k\Omega$ , and  $C = 1\mu F$ , then the steady-state current  $i(t)$ , in milliamperes (mA) is



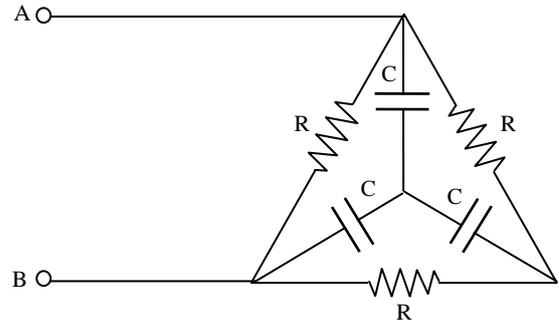
- (A)  $\sin(1000t) + \cos(1000t)$                       (B)  $\sin(1000t) + 3\cos(1000t)$   
 (C)  $2\sin(1000t) + 2\cos(1000t)$                       (D)  $3\sin(1000t) + \cos(1000t)$

**Key: (D)**

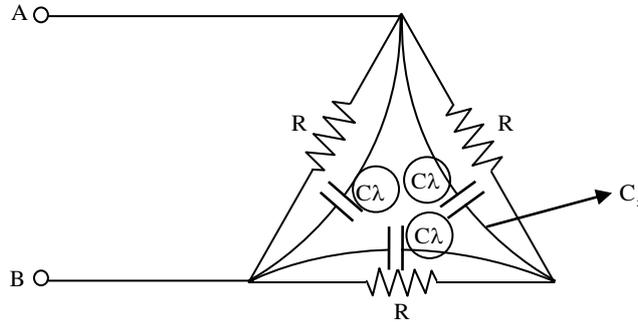
**Sol:** → It is given that  $V(t) = 2\sin 100t = \bar{V} = 2\angle 0^\circ$   
 $R = 1k\Omega, C = 1\mu F$

→ By observity the circuit we can say

$$\bar{I} = \frac{\bar{V}}{Z}$$



→ When each element of star network are same then its corresponding delta element are same and it becomes

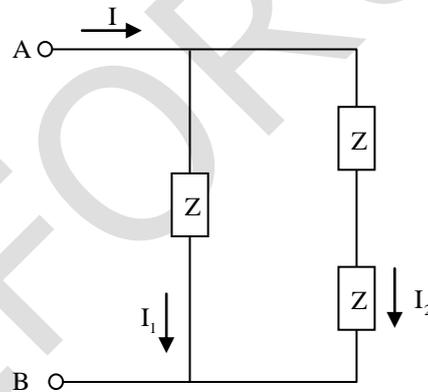


$Z_A = 3Z^*$ , but in capacitor case  $Z = \frac{1}{j\omega C}$ , So if the capacitor of star network are C each

then in its delta equivalent it becomes  $C/3 = C_x$

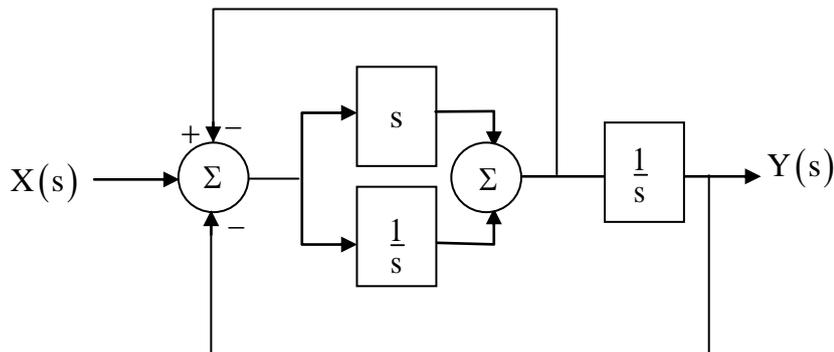
→ The network can be further redrawn as

$$\begin{aligned} \text{Where } Z &= R \parallel \frac{1}{j\omega C_x} = \frac{R / j\omega C_x}{R + \frac{1}{j\omega C_x}} = \frac{R}{1 + j\omega R C_x} \\ &= \frac{R}{1 + j\omega R \frac{C}{3}} = \frac{3R}{3 + j\omega R C} = \frac{3R}{3 + j} \end{aligned}$$



$$\begin{aligned} \rightarrow \bar{I} &= \bar{I}_1 + \bar{I}_2 = \frac{\bar{V}}{Z} + \frac{\bar{V}}{2Z} = \frac{2\bar{0}}{(3R/3 + j)} + \frac{2\bar{0}}{(65R/3 + j)} \\ &= \frac{3 + j}{3R} [2\bar{0} + 1\bar{0}] = \frac{3 + j}{R} (1\bar{0}) = \frac{[3\bar{0}] + [1\bar{90}]}{R} \\ &= 3\bar{0} + 1\bar{90} \text{mA } (\because 12 - 1000\Omega) = 3\sin 1000t + \sin(1000t + 90^\circ) \end{aligned}$$

54. The block diagram of a system is illustrated in the figure shown, where  $X(s)$  is the input and  $Y(s)$  is the output. The transfer function  $H(s) = \frac{Y(s)}{X(s)}$  is



(A)  $H(s) = \frac{s^2 + 1}{2s^2 + 1}$

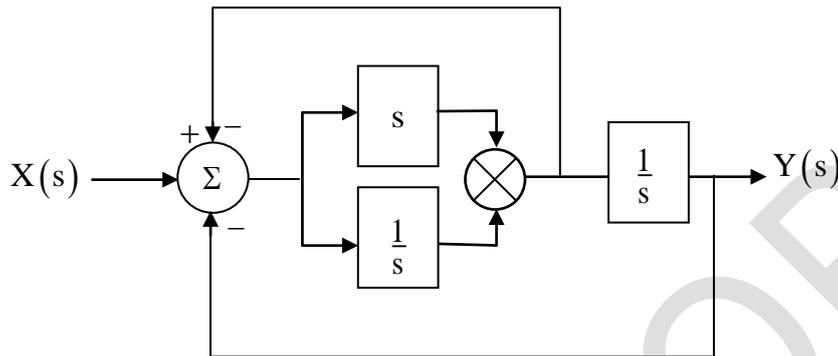
(B)  $H(s) = \frac{s^2 + 1}{s^3 + 2s^2 + s + 1}$

(C)  $H(s) = \frac{s + 1}{s^2 + s + 1}$

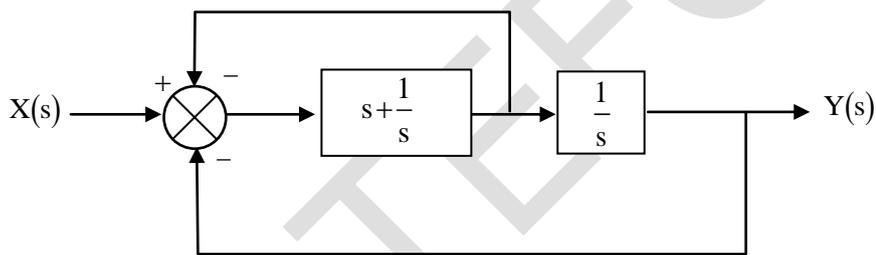
(D)  $H(s) = \frac{s^2 + 1}{s^3 + s^2 + s + 1}$

**Key: (B)**

**Sol:** Given block diagram



It can be reduced to

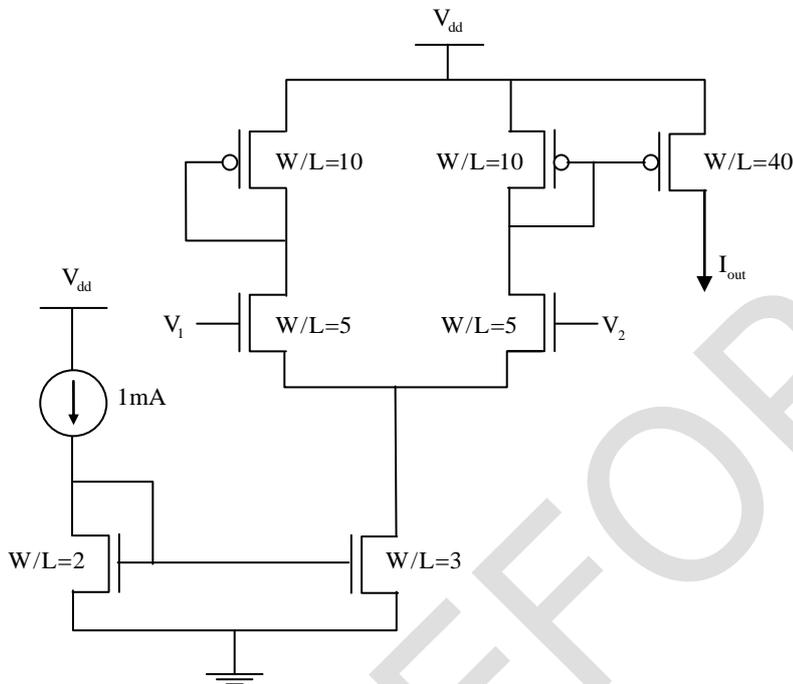


$$\frac{Y(s)}{X(s)} = \frac{\frac{(s^2 + 1)}{s} \times \frac{1}{s}}{1 + \frac{s^2 + 1}{s} + \frac{s^2 + 1}{s^2}} = \frac{\frac{(s^2 + 1)}{s^2}}{s^2 + (s^2 + 1)s + s^2 + 1}$$

$$= \frac{(s^2 + 1)}{s^2 + s^3 + s + s^2 + 1} = \frac{(s^2 + 1)}{s^3 + 2s^2 + s + 1}$$

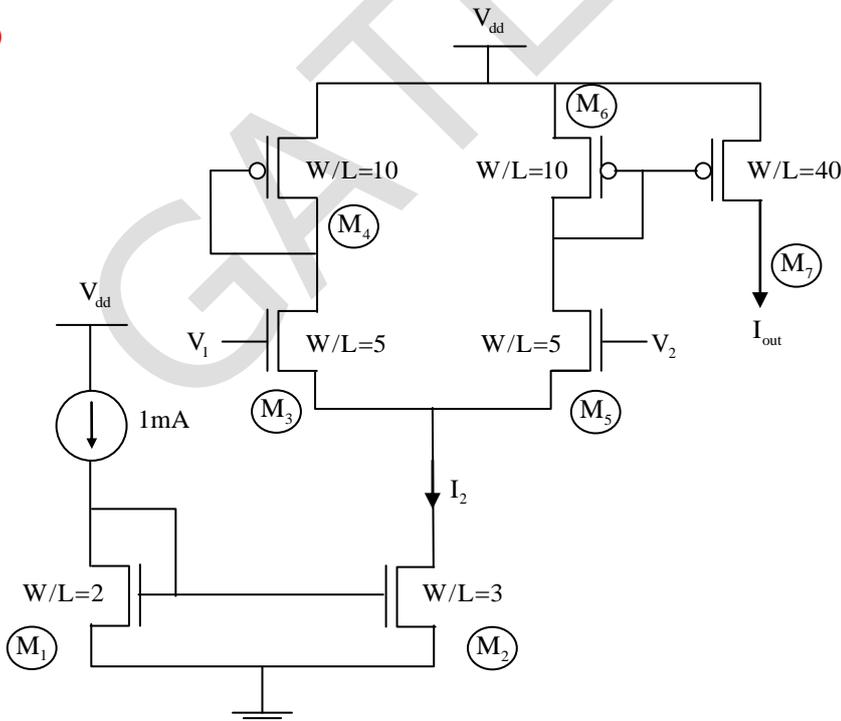
Hence, the transfer function  $H(s) = \frac{Y(s)}{X(s)}$  is  $\frac{(s^2 + 1)}{(s^3 + 2s^2 + s + 1)}$

55. In the circuit shown,  $V_1 = 0$  and  $V_2 = V_{dd}$ . The other relevant parameters are mentioned in the figure. Ignoring the effect of channel length modulation and the body effect, the value of  $I_{out}$  is \_\_\_\_ mA (rounded off to one decimal place).



**Key: (6)**

**Sol:**



$M_1$  and  $M_2$  have the same  $V_{gs}$

∴ Current flows in the ratio of W/L

$$\therefore I_2 = \left(\frac{3}{2}\right)^{(1\text{mA})} = 1.5\text{mA}$$

$V_1 = 0$ ; Therefore  $M_3$  is in cut off and entire  $I_2$  current flows through  $M_5$  branch.

$$\therefore I_5 = 1.5\text{mA}$$

$$I_{\text{out}} = \left(\frac{40}{10}\right)^{[I_5]} \quad [\text{Ratio of W/L}]$$

$$\therefore I_{\text{out}} = 4 \times 1.5\text{mA} = 6\text{mA}$$

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